

LM4562

Dual High Performance, High Fidelity Audio Operational Amplifier

General Description

The LM4562 is part of the ultra-low distortion, low noise, high slew rate operational amplifier series optimized and fully specified for high performance, high fidelity applications. Combining advanced leading-edge process technology with state-of-the-art circuit design, the LM4562 audio operational amplifiers deliver superior audio signal amplification for outstanding audio performance. The LM4562 combines extremely low voltage noise density ($2.7\text{nV}/\sqrt{\text{Hz}}$) with vanishingly low THD+N (0.00003%) to easily satisfy the most demanding audio applications. To ensure that the most challenging loads are driven without compromise, the LM4562 has a high slew rate of $\pm 20\text{V}/\mu\text{s}$ and an output current capability of $\pm 26\text{mA}$. Further, dynamic range is maximized by an output stage that drives $2\text{k}\Omega$ loads to within 1V of either power supply voltage and to within 1.4V when driving 600Ω loads.

The LM4562's outstanding CMRR (120dB), PSRR (120dB), and V_{OS} (0.1mV) give the amplifier excellent operational amplifier DC performance.

The LM4562 has a wide supply range of $\pm 2.5\text{V}$ to $\pm 17\text{V}$. Over this supply range the LM4562's input circuitry maintains excellent common-mode and power supply rejection, as well as maintaining its low input bias current. The LM4562 is unity gain stable. This Audio Operational Amplifier achieves outstanding AC performance while driving complex loads with values as high as 100pF .

The LM4562 is available in 8-lead narrow body SOIC, 8-lead Plastic DIP, and 8-lead Metal Can TO-99. Demonstration boards are available for each package.

Key Specifications

- Power Supply Voltage Range $\pm 2.5\text{V}$ to $\pm 17\text{V}$
- THD+N ($A_V = 1$, $V_{\text{OUT}} = 3V_{\text{RMS}}$, $f_{\text{IN}} = 1\text{kHz}$)

$R_L = 2\text{k}\Omega$	0.00003% (typ)
$R_L = 600\Omega$	0.00003% (typ)
■ Input Noise Density	$2.7\text{nV}/\sqrt{\text{Hz}}$ (typ)
■ Slew Rate	$\pm 20\text{V}/\mu\text{s}$ (typ)
■ Gain Bandwidth Product	55MHz (typ)
■ Open Loop Gain ($R_L = 600\Omega$)	140dB (typ)
■ Input Bias Current	10nA (typ)
■ Input Offset Voltage	0.1mV (typ)
■ DC Gain Linearity Error	0.000009%

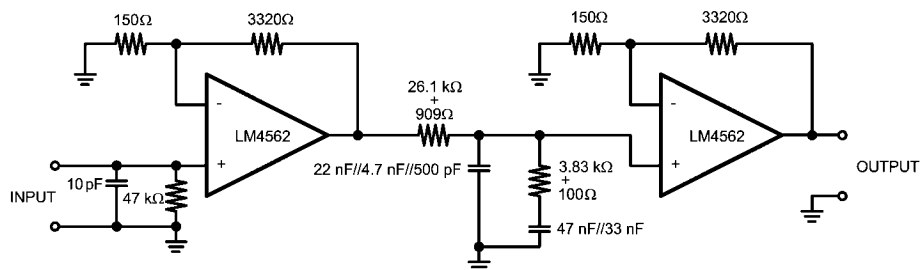
Features

- Easily drives 600Ω loads
- Optimized for superior audio signal fidelity
- Output short circuit protection
- PSRR and CMRR exceed 120dB (typ)
- SOIC, DIP, TO-99 metal can packages

Applications

- Ultra high quality audio amplification
- High fidelity preamplifiers
- High fidelity multimedia
- State of the art phono pre amps
- High performance professional audio
- High fidelity equalization and crossover networks
- High performance line drivers
- High performance line receivers
- High fidelity active filters

Typical Application



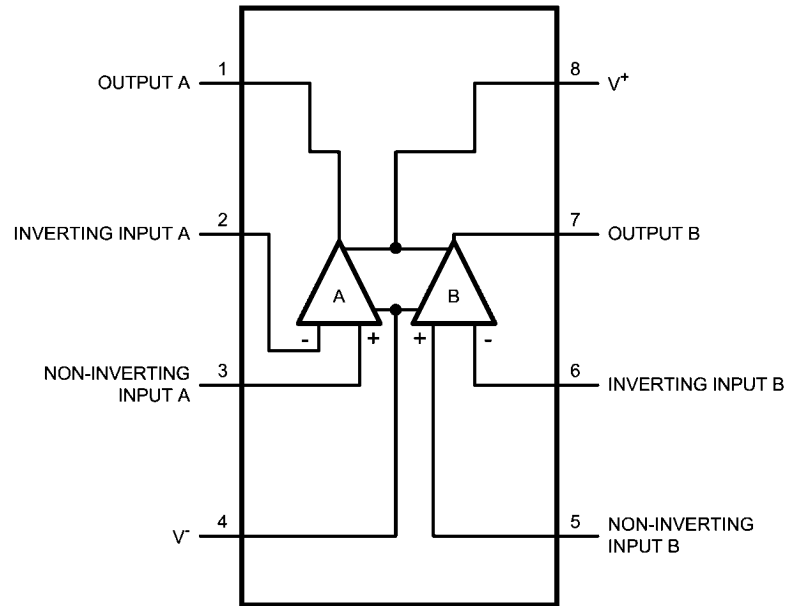
Note: 1% metal film resistors, 5% polypropylene capacitors

Passively Equalized RIAA Phono Preamplifier

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Connection Diagrams

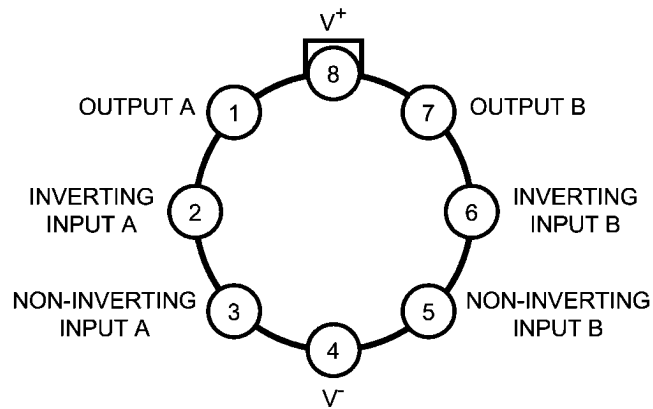
Dual-In-Line Package



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Order Number LM4562MA
See NS Package Number — M08A
Order Number LM4562NA
See NS Package Number — N08E

Metal Can



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Order Number LM4562HA
See NS Package Number — H08C

Absolute Maximum Ratings (Notes 1, 2)

If Military/Aerospace specified devices are required,
please contact the National Semiconductor Sales Office/
Distributors for availability and specifications.

Power Supply Voltage ($V_S = V^+ - V^-$)	36V
Storage Temperature	-65°C to 150°C
Input Voltage (V^-) - 0.7V to (V^+) + 0.7V	
Output Short Circuit (Note 3)	Continuous
Power Dissipation	Internally Limited
ESD Susceptibility (Note 4)	2000V
ESD Susceptibility (Note 5)	

Pins 1, 4, 7 and 8	200V
Pins 2, 3, 5 and 6	100V
Junction Temperature	150°C
Thermal Resistance	
θ_{JA} (SO)	145°C/W
θ_{JA} (NA)	102°C/W
θ_{JA} (HA)	150°C/W
θ_{JC} (HA)	35°C/W
Temperature Range	
$T_{MIN} \leq T_A \leq T_{MAX}$	-40°C $\leq T_A \leq$ 85°C
Supply Voltage Range	$\pm 2.5V \leq V_S \leq \pm 17V$

Electrical Characteristics for the LM4562

Symbol	Parameter	Conditions	LM4562		Units (Limits)
			Typical	Limit	
			(Note 6)	(Note 7)	
THD+N	Total Harmonic Distortion + Noise	$A_V = 1$, $V_{OUT} = 3V_{rms}$ $R_L = 2k\Omega$ $R_L = 600\Omega$	0.00003 0.00003	0.00009	% (max)
IMD	Intermodulation Distortion	$A_V = 1$, $V_{OUT} = 3V_{RMS}$ Two-tone, 60Hz & 7kHz 4:1	0.00005		%
GBWP	Gain Bandwidth Product		55	45	MHz (min)
SR	Slew Rate		± 20	± 15	V/ μ s (min)
FPBW	Full Power Bandwidth	$V_{OUT} = 1V_{P-P}$, -3dB referenced to output magnitude at $f = 1kHz$	10		MHz
t_s	Settling time	$A_V = -1$, 10V step, $C_L = 100pF$ 0.1% error range	1.2		μ s
e_n	Equivalent Input Noise Voltage	$f_{BW} = 20Hz$ to 20kHz	0.34	0.65	μV_{RMS} (max)
	Equivalent Input Noise Density	$f = 1kHz$ $f = 10Hz$	2.7 6.4	4.7	nV/ \sqrt{Hz} (max)
i_n	Current Noise Density	$f = 1kHz$ $f = 10Hz$	1.6 3.1		pA/ \sqrt{Hz}
V_{OS}	Offset Voltage		± 0.1	± 0.7	mV (max)
$\Delta V_{OS}/\Delta Temp$	Average Input Offset Voltage Drift vs Temperature	-40°C $\leq T_A \leq$ 85°C	0.2		$\mu V/^\circ C$
PSRR	Average Input Offset Voltage Shift vs Power Supply Voltage	$\Delta V_S = 20V$ (Note 8)	120	110	dB (min)
ISO_{CH-CH}	Channel-to-Channel Isolation	$f_{IN} = 1kHz$ $f_{IN} = 20kHz$	118 112		dB
I_B	Input Bias Current	$V_{CM} = 0V$	10	72	nA (max)
$\Delta I_{OS}/\Delta Temp$	Input Bias Current Drift vs Temperature	-40°C $\leq T_A \leq$ 85°C	0.1		nA/ $^\circ C$
I_{OS}	Input Offset Current	$V_{CM} = 0V$	11	65	nA (max)
V_{IN-CM}	Common-Mode Input Voltage Range		+14.1 -13.9	(V^+) - 2.0 (V^-) + 2.0	V (min)
CMRR	Common-Mode Rejection	-10V < V_{cm} < 10V	120	110	dB (min)
Z_{IN}	Differential Input Impedance		30		k Ω
	Common Mode Input Impedance	-10V < V_{cm} < 10V	1000		M Ω

Symbol	Parameter	Conditions	LM4562		Units (Limits)
			Typical	Limit	
			(Note 6)	(Note 7)	
A_{VOL}	Open Loop Voltage Gain	$-10V < V_{out} < 10V, R_L = 600\Omega$	140	125	dB (min)
		$-10V < V_{out} < 10V, R_L = 2k\Omega$	140		
		$-10V < V_{out} < 10V, R_L = 10k\Omega$	140		
V_{OUTMAX}	Maximum Output Voltage Swing	$R_L = 600\Omega$	± 13.6	± 12.5	V (min)
		$R_L = 2k\Omega$	± 14.0		
		$R_L = 10k\Omega$	± 14.1		
I_{OUT}	Output Current	$R_L = 600\Omega, V_S = \pm 17V$	± 26	± 23	mA (min)
I_{OUT-CC}	Instantaneous Short Circuit Current		+53 -42		mA
R_{OUT}	Output Impedance	$f_{IN} = 10kHz$ Closed-Loop Open-Loop	0.01 13		Ω
C_{LOAD}	Capacitive Load Drive Overshoot	100pF	16		%
I_S	Total Quiescent Current	$I_{OUT} = 0mA$	10	12	mA (max)

Note 1: *Absolute Maximum Ratings* indicate limits beyond which damage to the device may occur.

Note 2: Operating Ratings indicate conditions for which the device is functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

Note 3: Amplifier output connected to GND, any number of amplifiers within a package.

Note 4: Human body model, 100pF discharged through a 1.5k Ω resistor.

Note 5: Machine Model ESD test is covered by specification EIAJ IC-121-1981. A 200pF cap is charged to the specified voltage and then discharged directly into the IC with no external series resistor (resistance of discharge path must be under 50 Ω).

Note 6: Typical specifications are specified at +25°C and represent the most likely parametric norm.

Note 7: Tested limits are guaranteed to National's AOQL (Average Outgoing Quality Level).

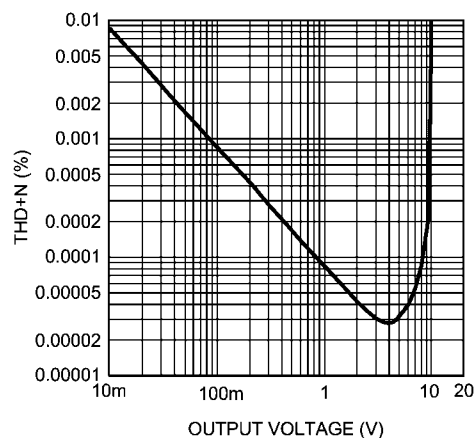
Note 8: PSRR is measured as follows: V_{OS} is measured at two supply voltages, $\pm 5V$ and $\pm 15V$. $PSRR = |20\log(\Delta V_{OS}/\Delta V_S)|$.

Typical Performance Characteristics

THD+N vs Output Voltage

$V_{CC} = 15V, V_{EE} = -15V$

$R_L = 2k\Omega$

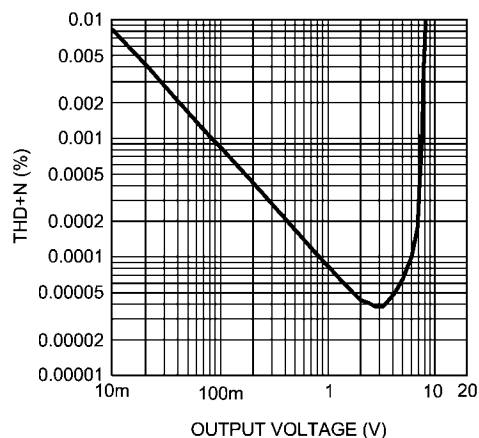


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THD+N vs Output Voltage

$V_{CC} = 12V, V_{EE} = -12V$

$R_L = 2k\Omega$

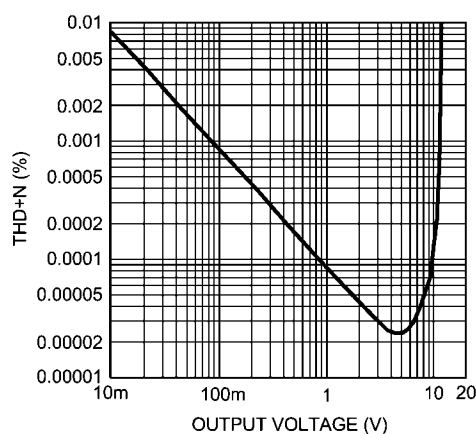


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THD+N vs Output Voltage

$V_{CC} = 17V, V_{EE} = -17V$

$R_L = 2k\Omega$

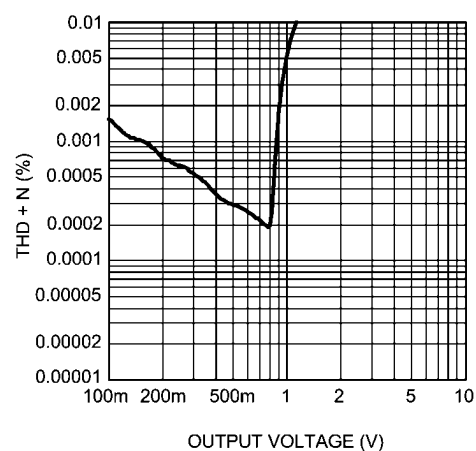


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THD+N vs Output Voltage

$V_{CC} = 2.5V, V_{EE} = -2.5V$

$R_L = 2k\Omega$

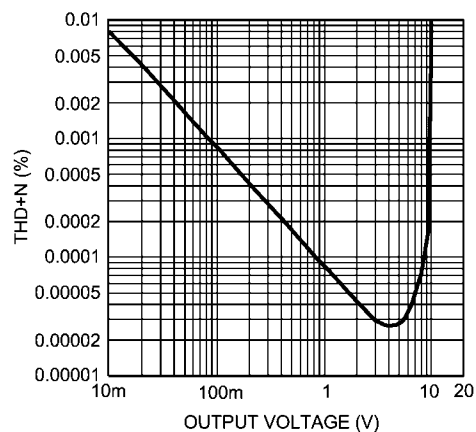


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THD+N vs Output Voltage

$V_{CC} = 15V, V_{EE} = -15V$

$R_L = 600\Omega$

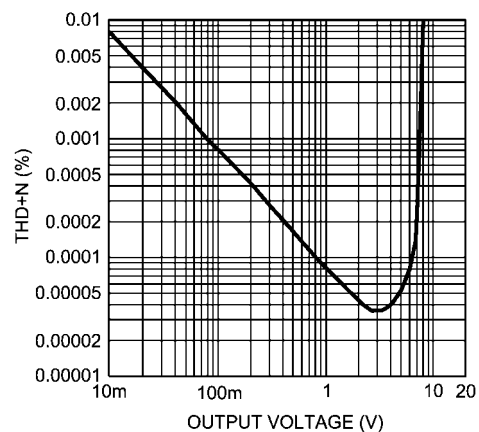


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THD+N vs Output Voltage

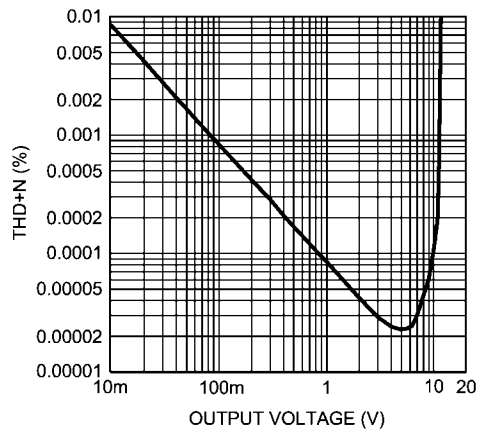
$V_{CC} = 12V, V_{EE} = -12V$

$R_L = 600\Omega$



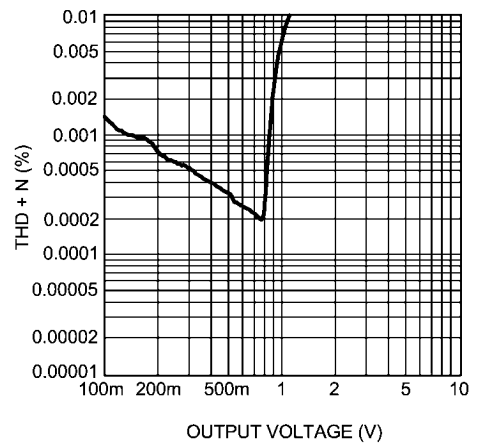
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THD+N vs Output Voltage
 $V_{CC} = 17V$, $V_{EE} = -17V$
 $R_L = 600\Omega$



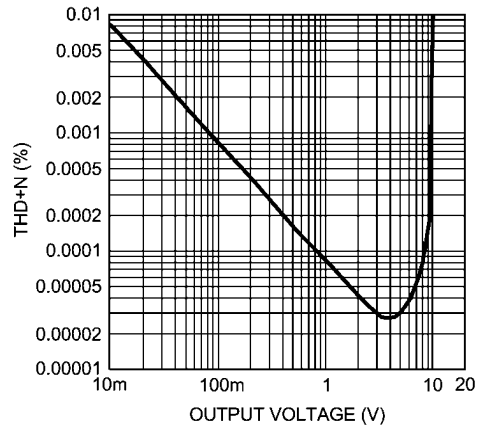
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THD+N vs Output Voltage
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 600\Omega$



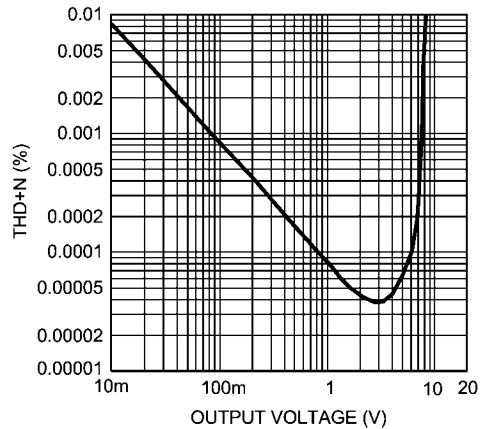
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THD+N vs Output Voltage
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 10k\Omega$



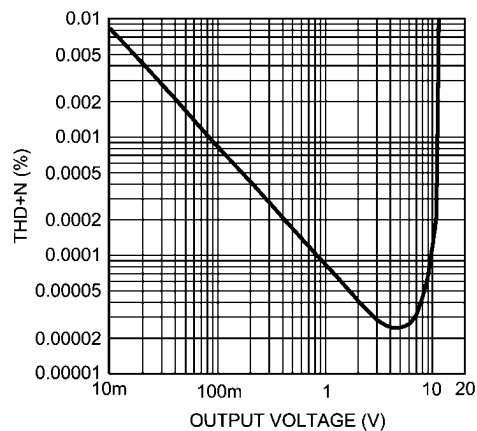
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THD+N vs Output Voltage
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 $R_L = 10k\Omega$



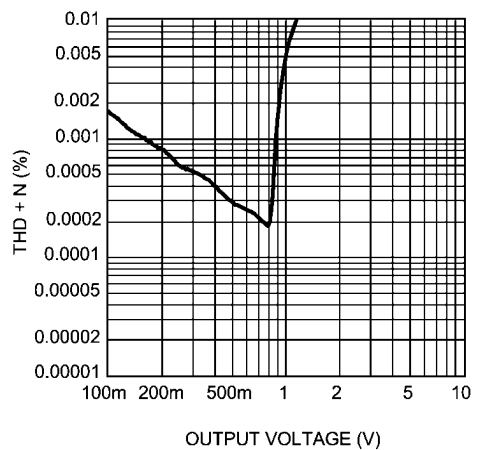
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THD+N vs Output Voltage
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 $R_L = 10k\Omega$



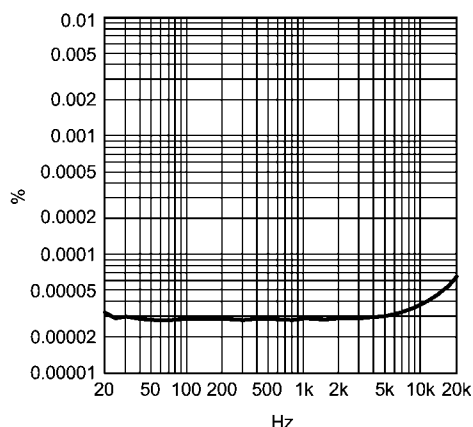
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THD+N vs Output Voltage
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 $R_L = 10k\Omega$



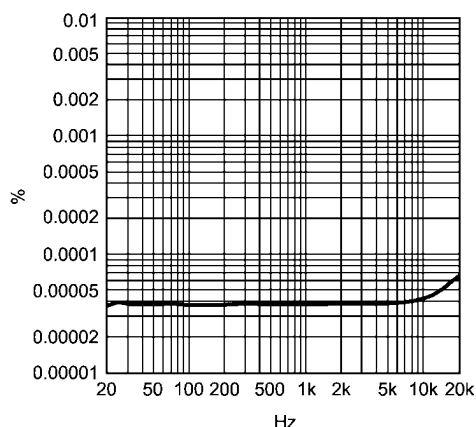
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THD+N vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 3V_{RMS}$
 $R_L = 2k\Omega$



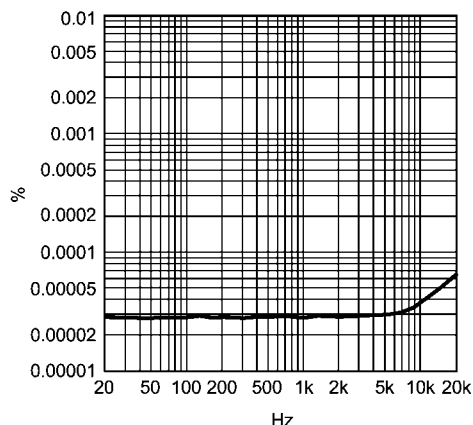
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THD+N vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 3V_{RMS}$
 $R_L = 2k\Omega$



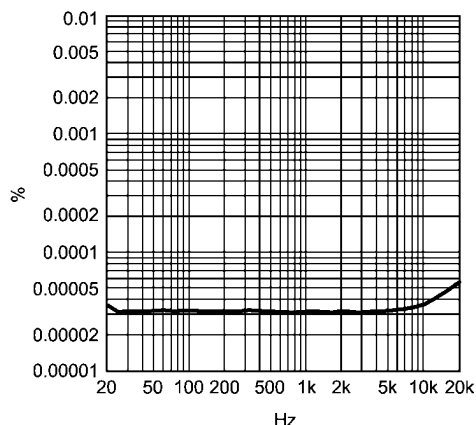
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THD+N vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 3V_{RMS}$
 $R_L = 2k\Omega$



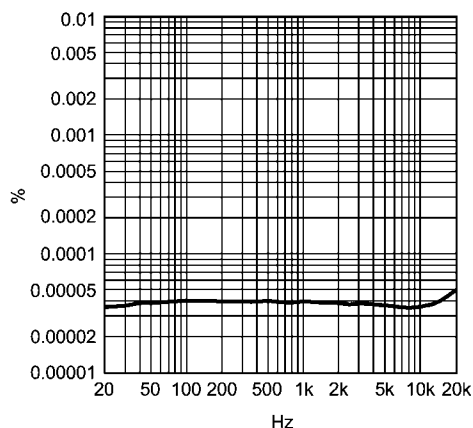
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THD+N vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 3V_{RMS}$
 $R_L = 600\Omega$



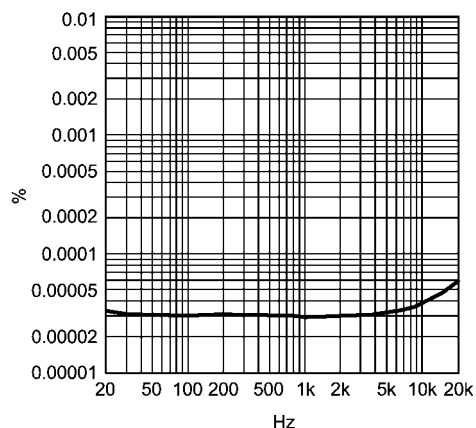
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THD+N vs Frequency
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 $R_L = 600\Omega$



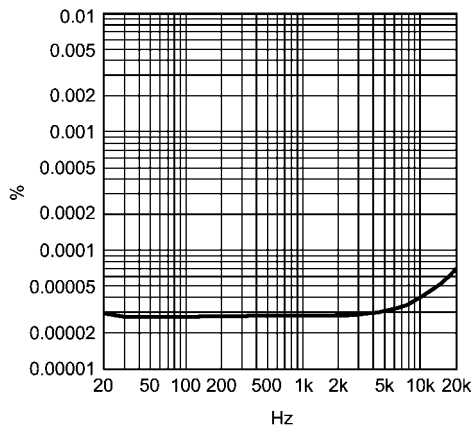
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THD+N vs Frequency
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 $R_L = 600\Omega$



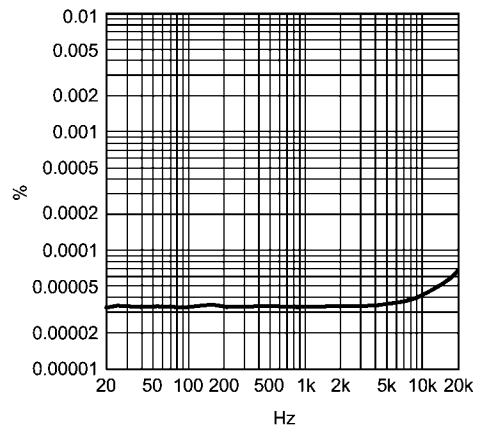
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THD+N vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 3V_{RMS}$
 $R_L = 10k\Omega$



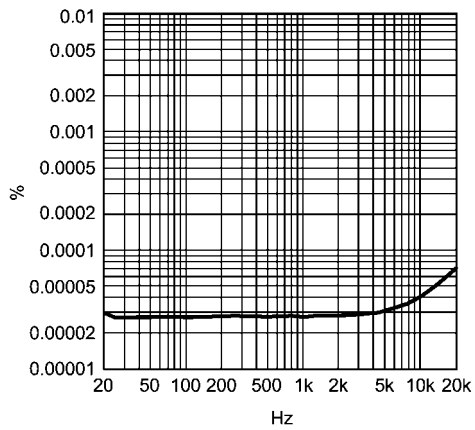
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THD+N vs Frequency
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 $R_L = 10k\Omega$



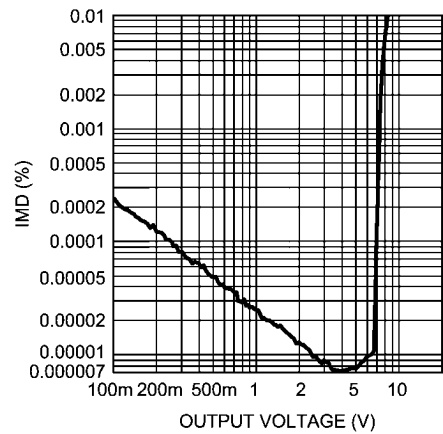
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THD+N vs Frequency
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 $R_L = 10k\Omega$



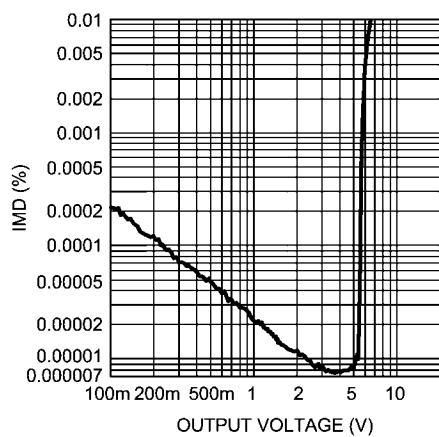
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IMD vs Output Voltage
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 2k\Omega$



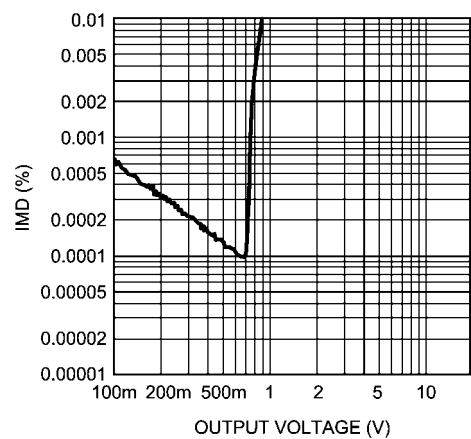
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IMD vs Output Voltage
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 2k\Omega$



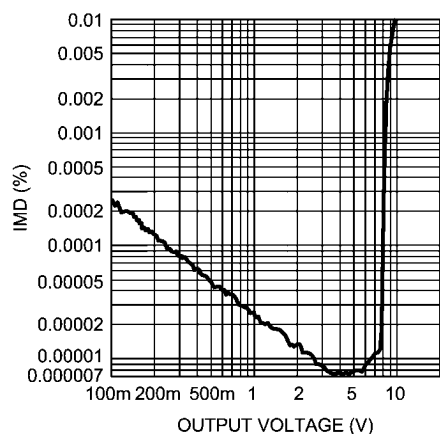
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IMD vs Output Voltage
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 2k\Omega$



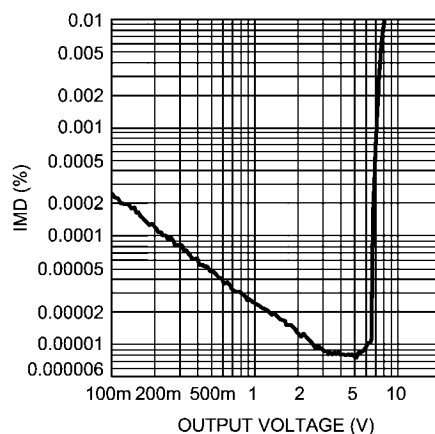
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IMD vs Output Voltage
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 $R_L = 2k\Omega$



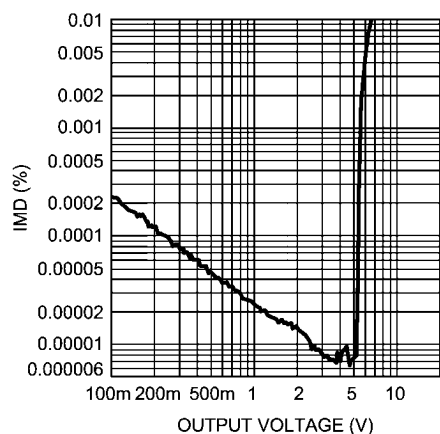
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IMD vs Output Voltage
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 600\Omega$



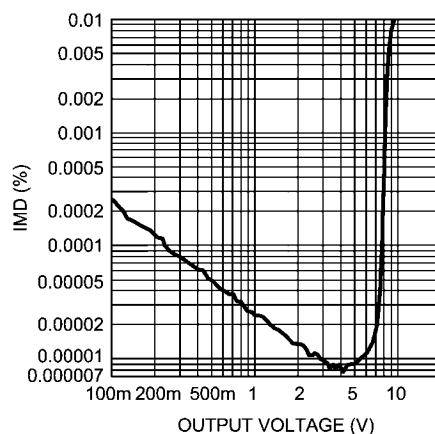
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IMD vs Output Voltage
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 600\Omega$



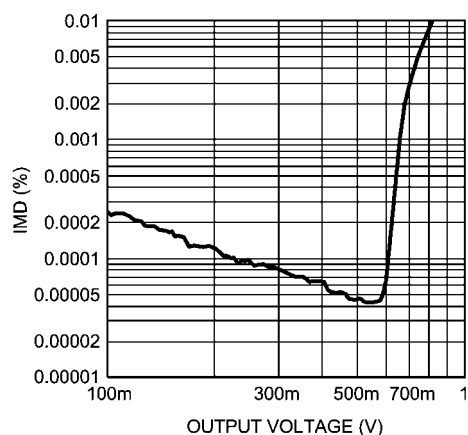
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IMD vs Output Voltage
 $V_{CC} = 17V$, $V_{EE} = -17V$
 $R_L = 600\Omega$



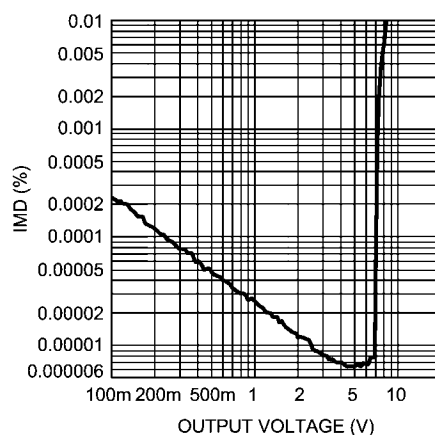
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IMD vs Output Voltage
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 600\Omega$



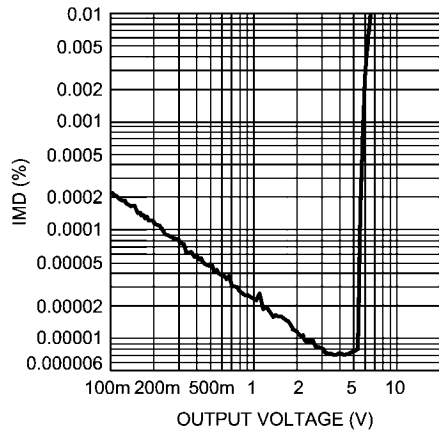
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IMD vs Output Voltage
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 10k\Omega$



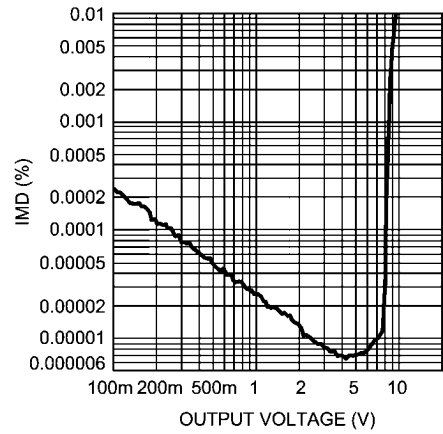
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IMD vs Output Voltage
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 $R_L = 10k\Omega$



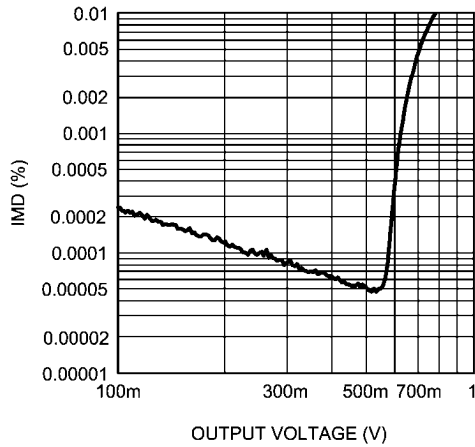
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IMD vs Output Voltage
 $V_{CC} = 17V$, $V_{EE} = -17V$
 $R_L = 10k\Omega$



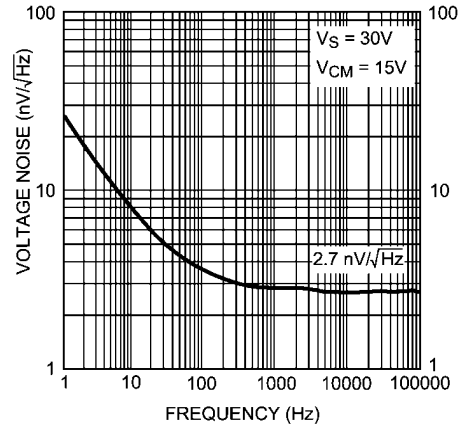
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IMD vs Output Voltage
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 10k\Omega$



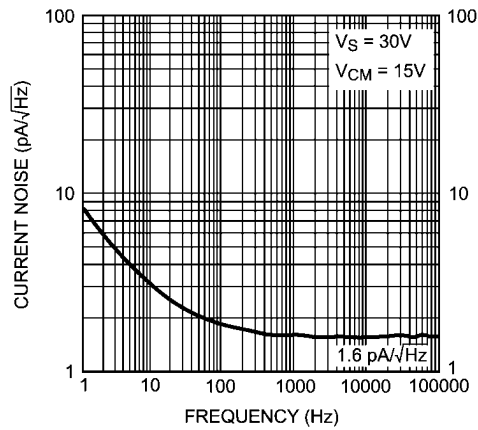
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Voltage Noise Density vs Frequency



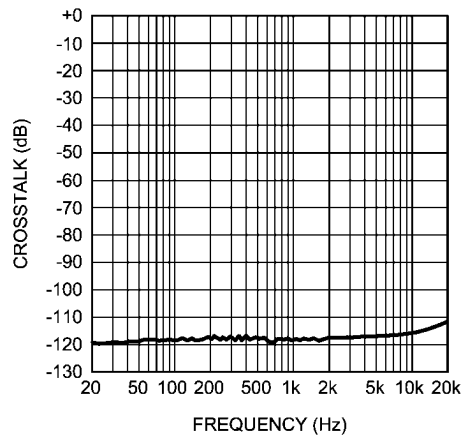
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Current Noise Density vs Frequency



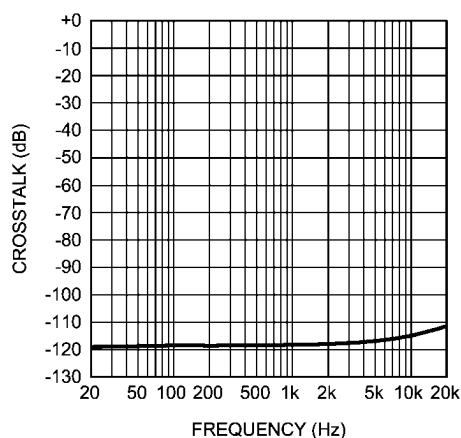
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Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 2k\Omega$



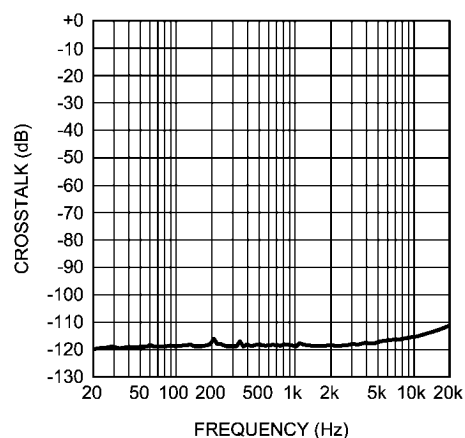
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Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 2k\Omega$



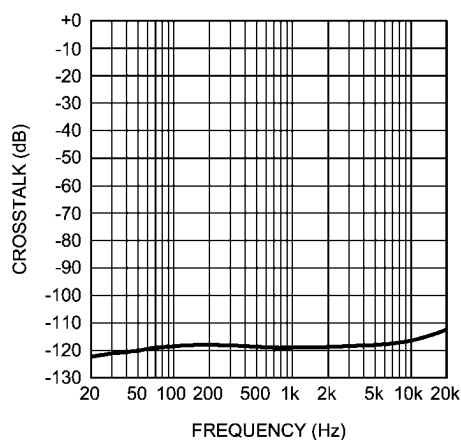
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Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 2k\Omega$



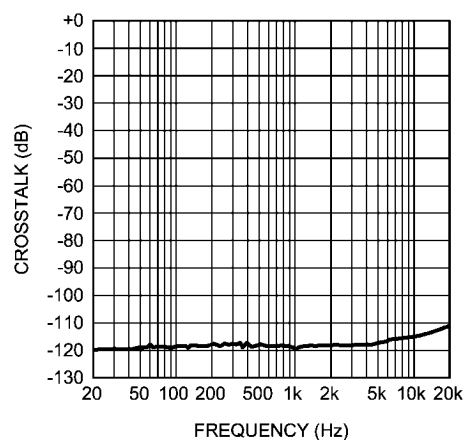
201572c6

Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 2k\Omega$



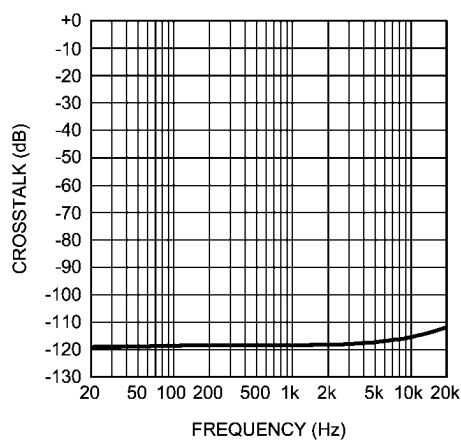
201572c7

Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 2k\Omega$



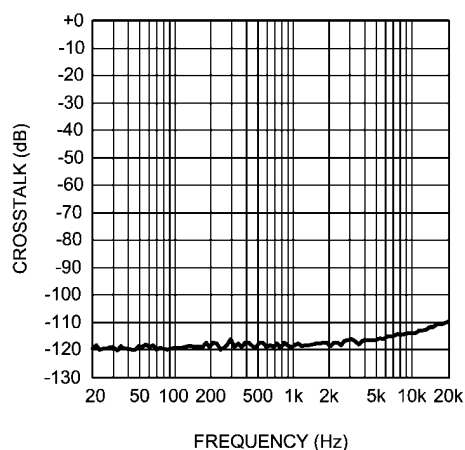
201572d0

Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 2k\Omega$



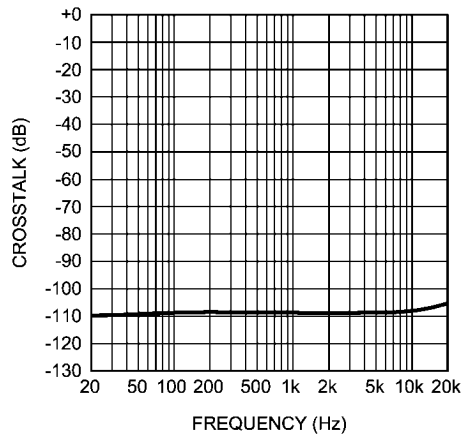
201572d1

Crosstalk vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$, $V_{OUT} = 1V_{RMS}$
 $A_V = 0dB$, $R_L = 2k\Omega$



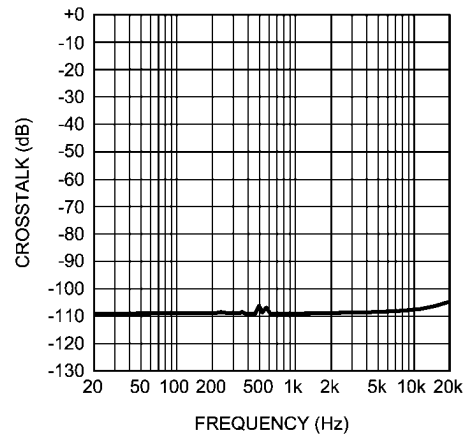
201572n8

Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 600\Omega$



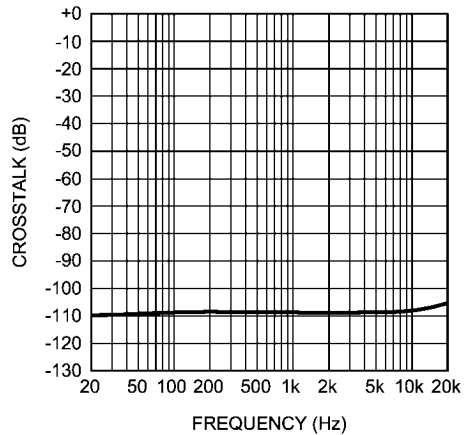
201572d6

Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 600\Omega$



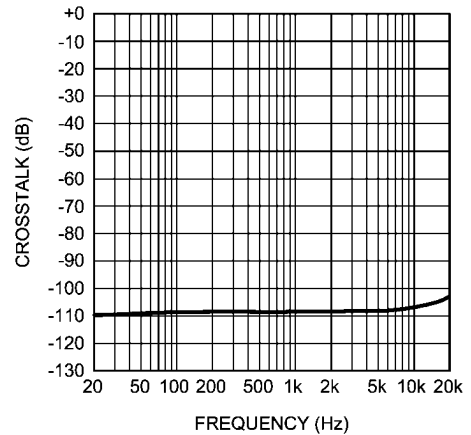
201572d7

Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 600\Omega$



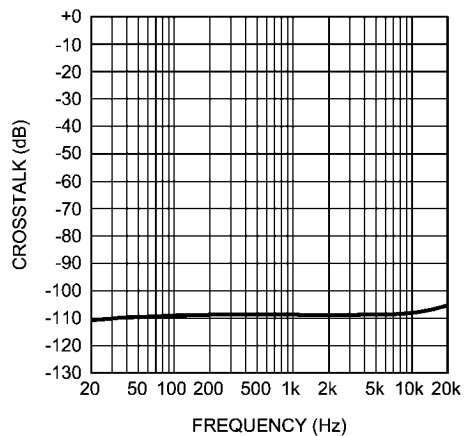
201572d4

Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 600\Omega$



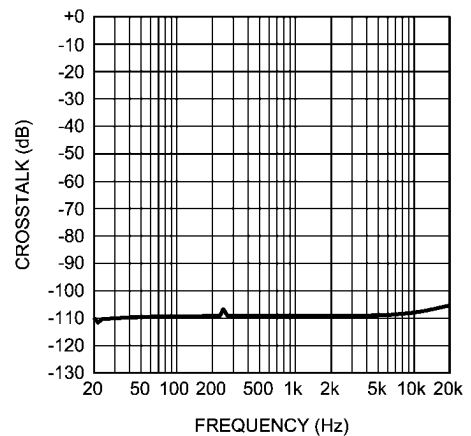
201572d5

Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 600\Omega$



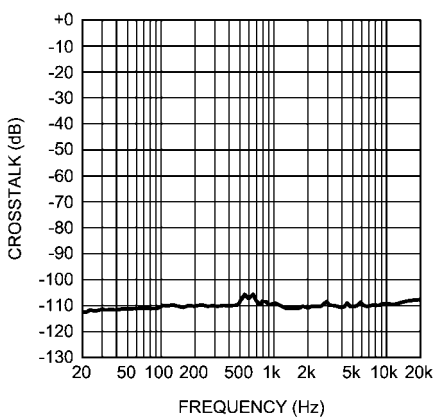
201572d8

Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 600\Omega$



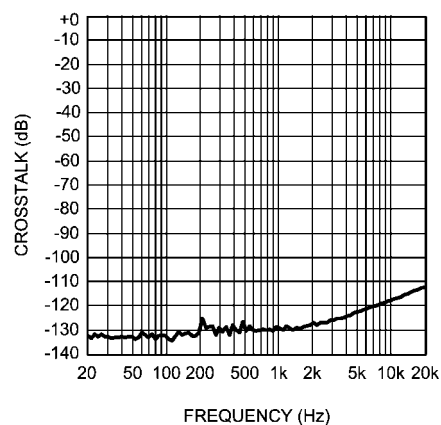
201572d9

Crosstalk vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$, $V_{OUT} = 1V_{RMS}$
 $A_V = 0dB$, $R_L = 600\Omega$



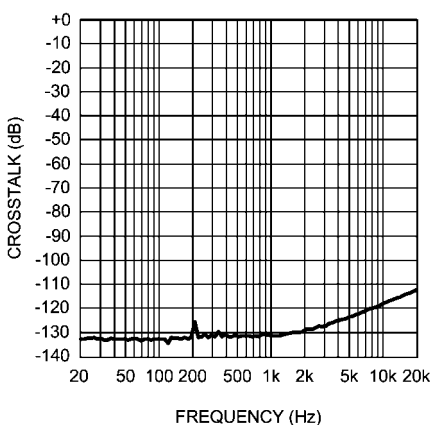
201572d2

Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



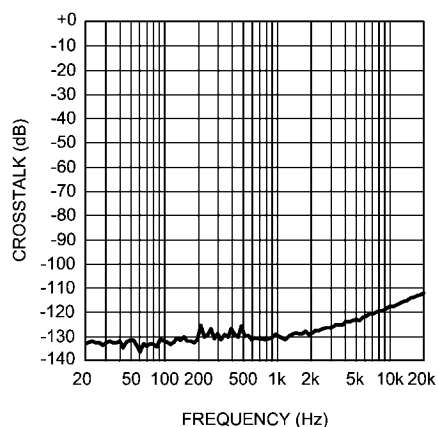
201572o0

Crosstalk vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



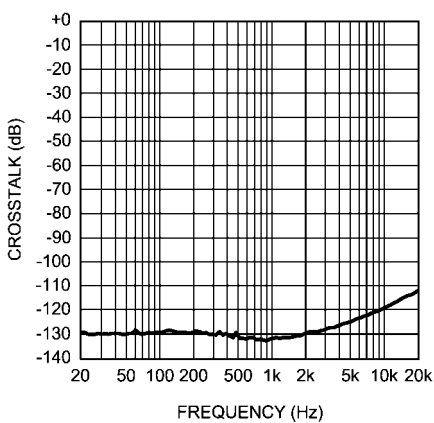
201572n7

Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



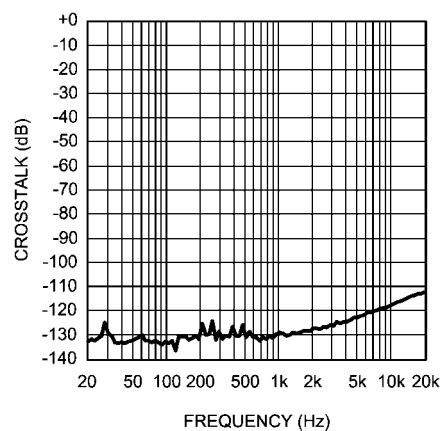
201572n9

Crosstalk vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



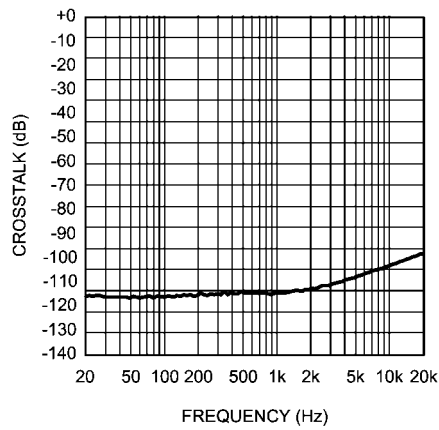
201572n6

Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 3V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



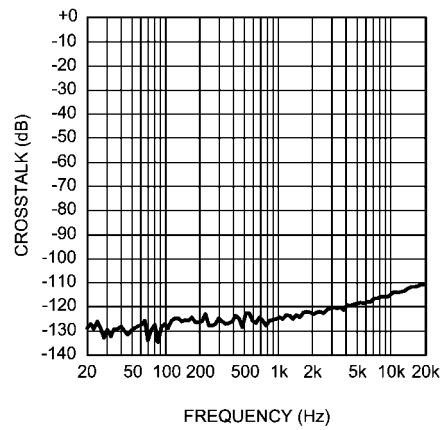
201572n5

Crosstalk vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$, $V_{OUT} = 10V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



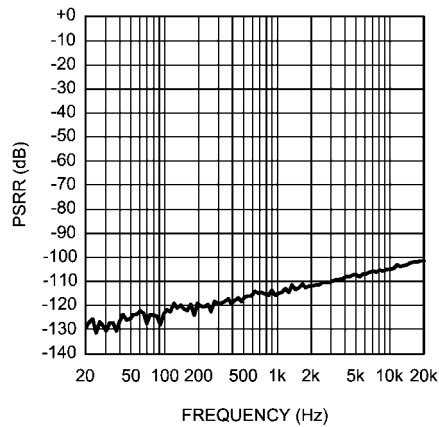
201572n3

Crosstalk vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$, $V_{OUT} = 1V_{RMS}$
 $A_V = 0dB$, $R_L = 10k\Omega$



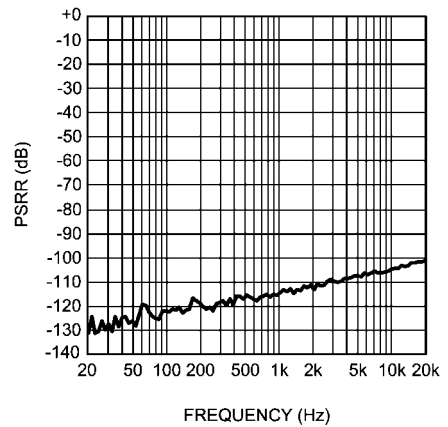
201572n4

PSRR+ vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 2k\Omega$, $V_{RIPPLE} = 200mV_{pp}$



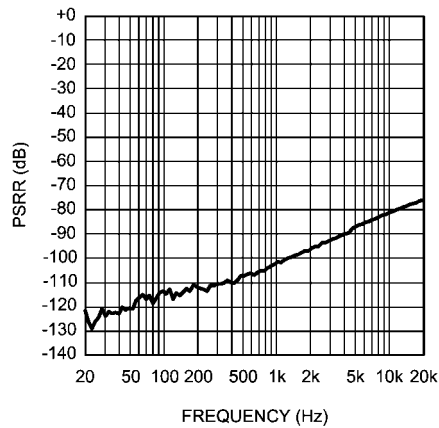
201572o1

PSRR- vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 2k\Omega$, $V_{RIPPLE} = 200mV_{pp}$



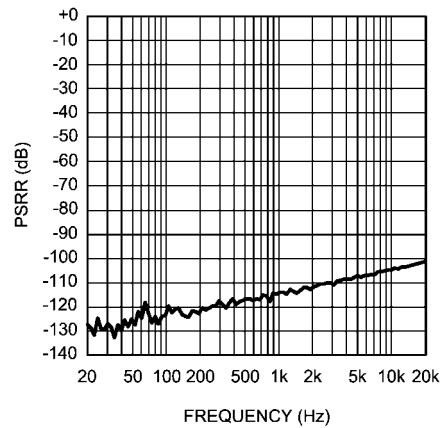
201572n2

PSRR+ vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 2k\Omega$, $V_{RIPPLE} = 200mV_{pp}$

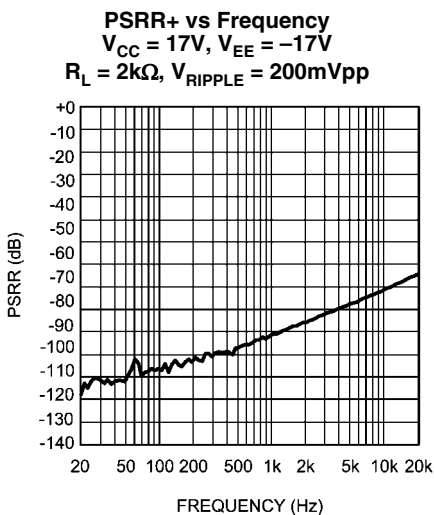


201572n1

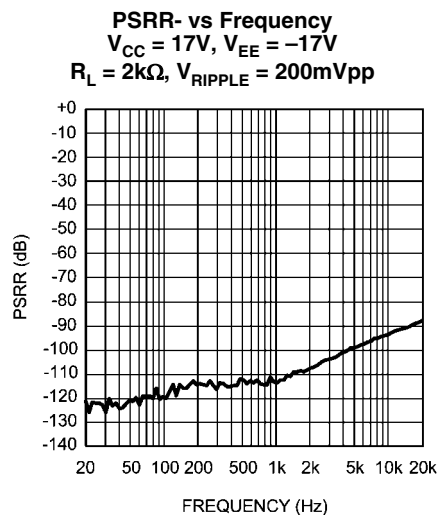
PSRR- vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 2k\Omega$, $V_{RIPPLE} = 200mV_{pp}$



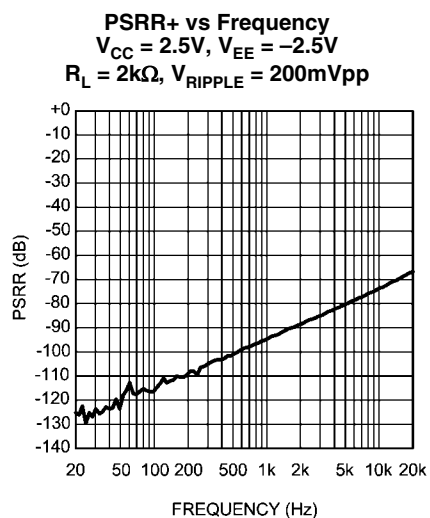
201572n0



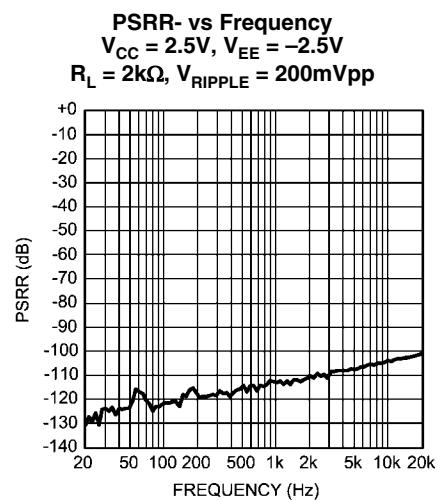
201572m9



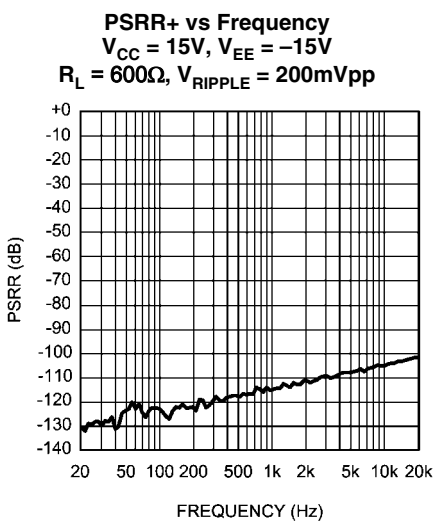
201572o3



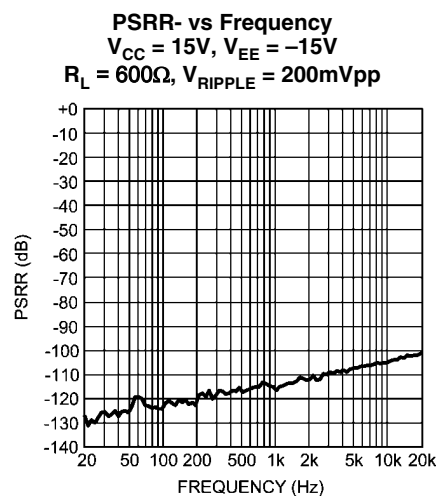
201572m8



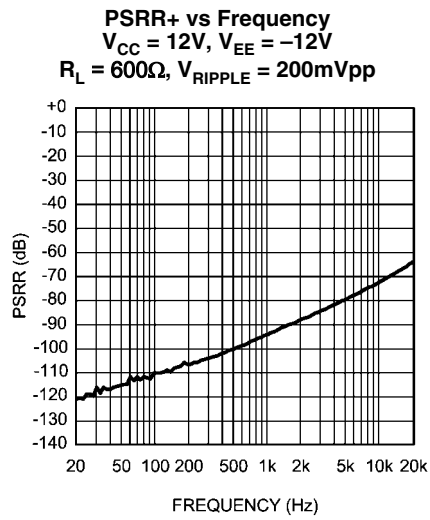
201572o6



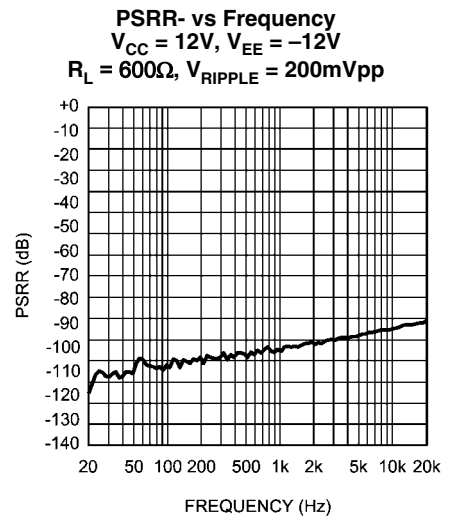
201572o2



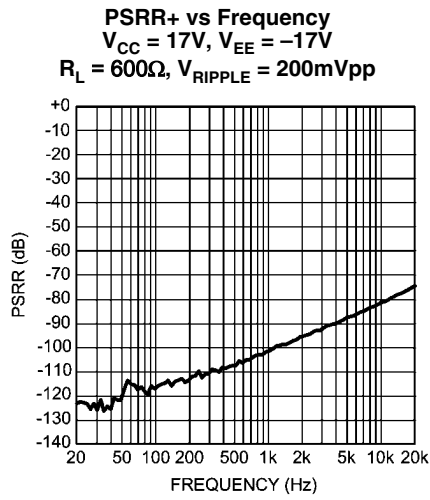
201572o7



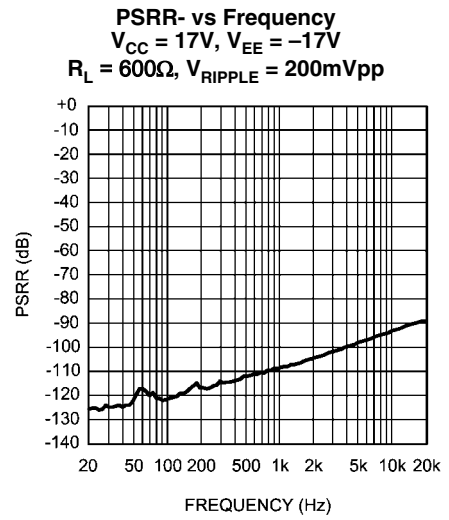
201572m7



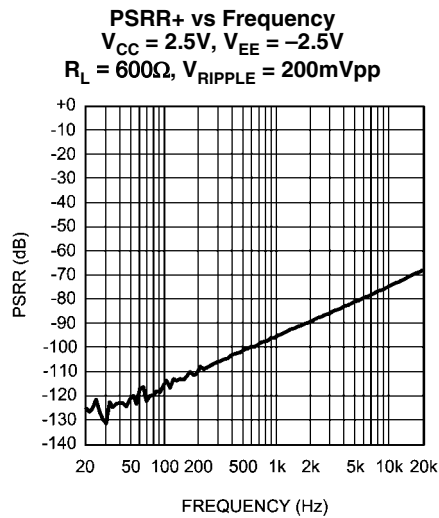
201572o4



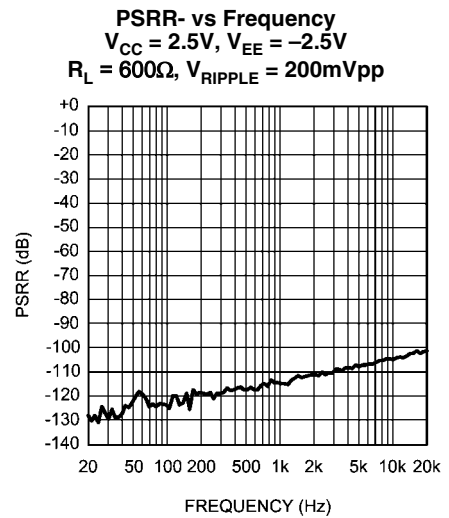
201572o5



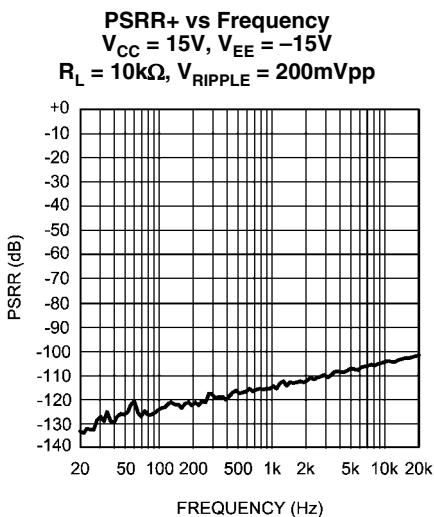
201572m6



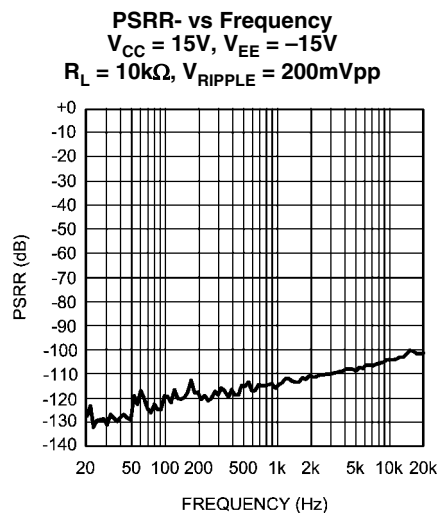
201572m5



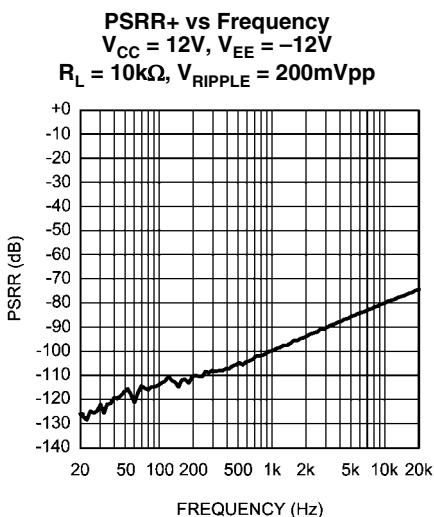
201572m4



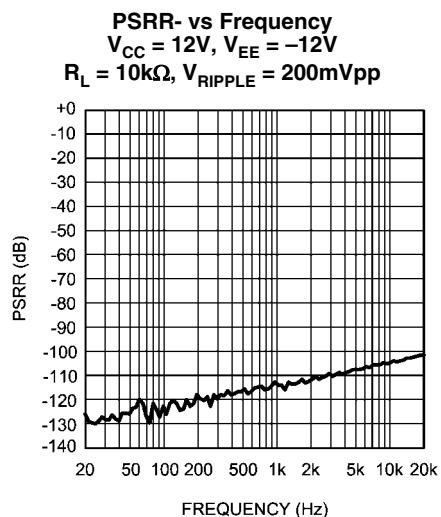
201572m3



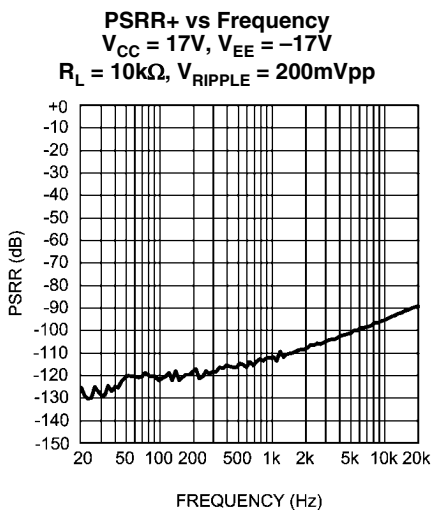
201572m2



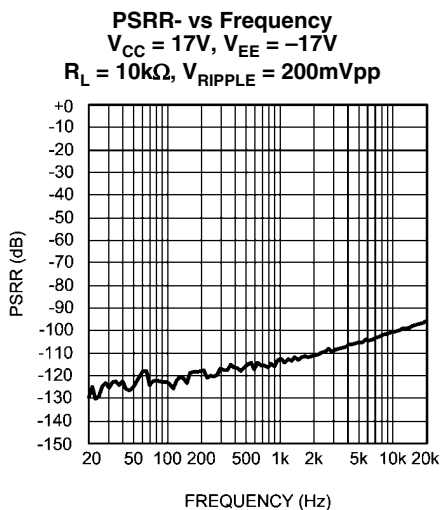
201572m1



201572m0

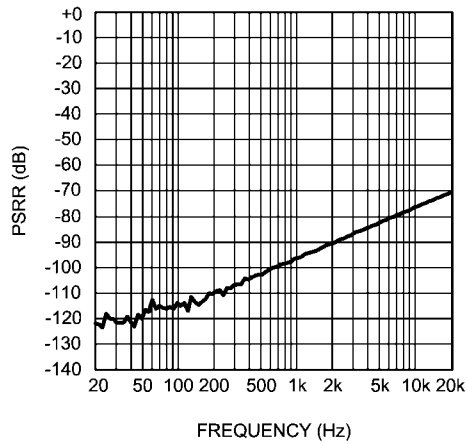


201572i9



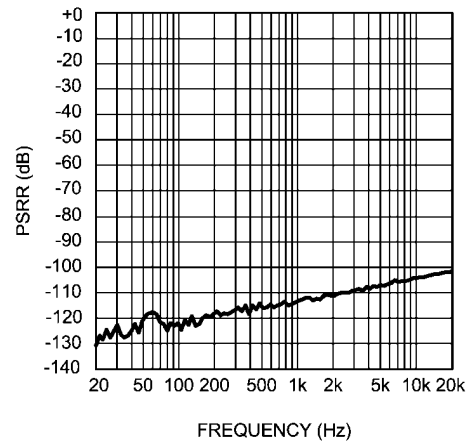
201572i8

PSRR+ vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 10k\Omega$, $V_{RIPPLE} = 200mV_{pp}$



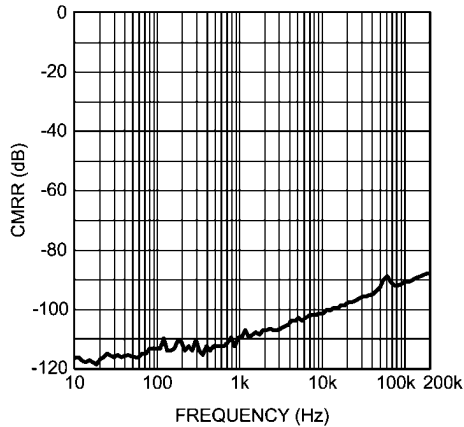
20157217

PSRR- vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 10k\Omega$, $V_{RIPPLE} = 200mV_{pp}$



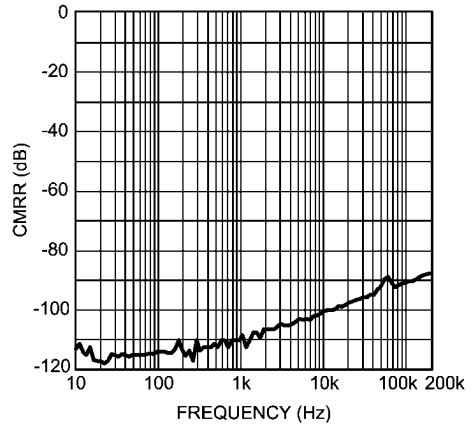
20157215

CMRR vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 2k\Omega$



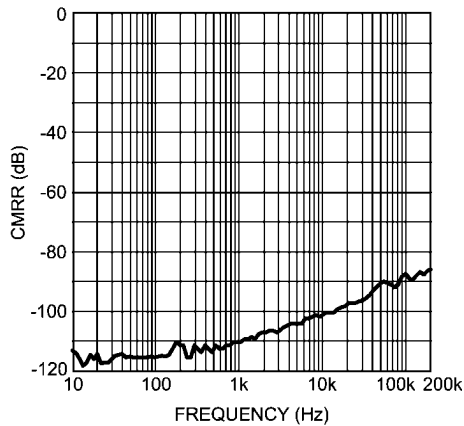
201572g0

CMRR vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 2k\Omega$



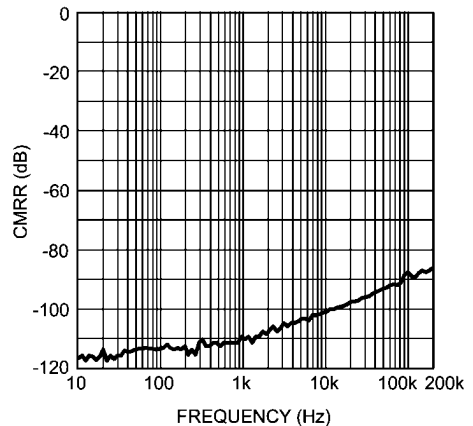
20157217

CMRR vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$
 $R_L = 2k\Omega$



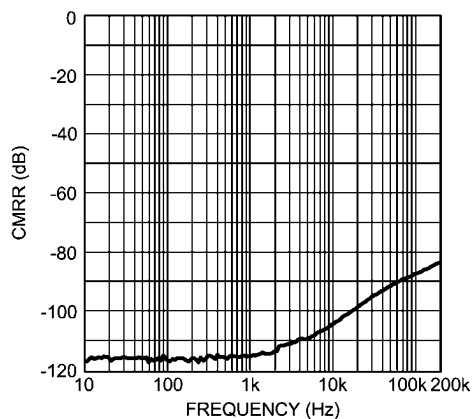
201572g3

CMRR vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 2k\Omega$



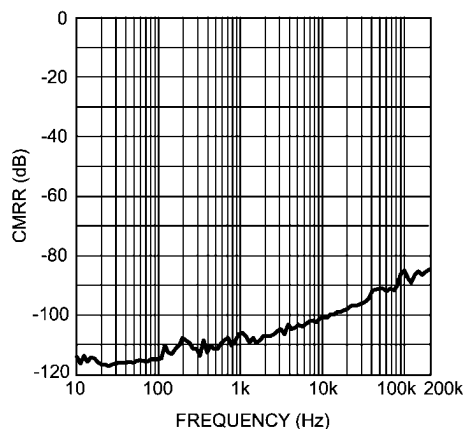
201572f4

CMRR vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 600\Omega$



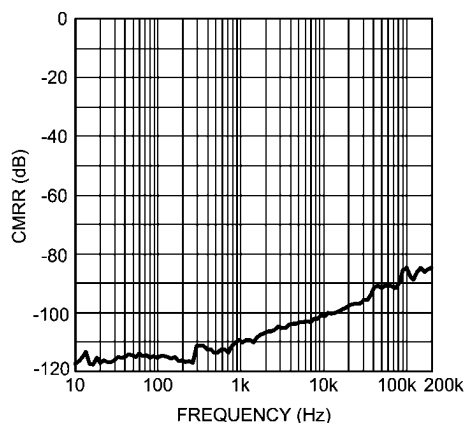
201572o9

CMRR vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 600\Omega$



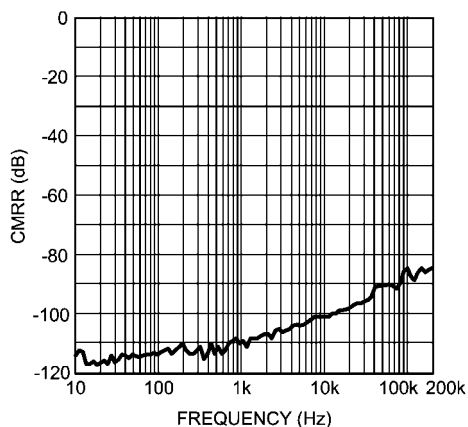
201572f9

CMRR vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$
 $R_L = 600\Omega$



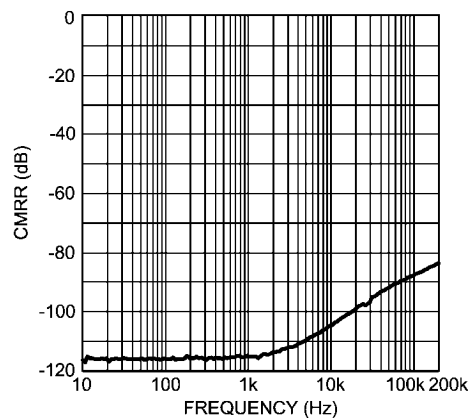
201572g5

CMRR vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 600\Omega$



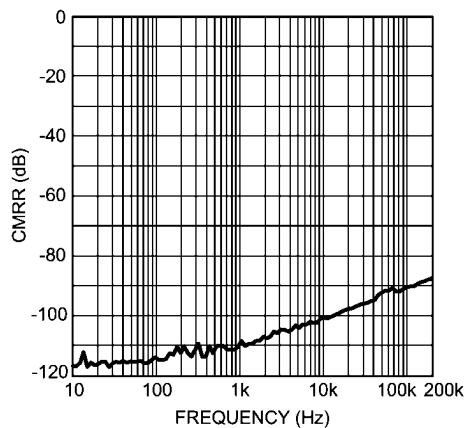
201572f6

CMRR vs Frequency
 $V_{CC} = 15V$, $V_{EE} = -15V$
 $R_L = 10k\Omega$



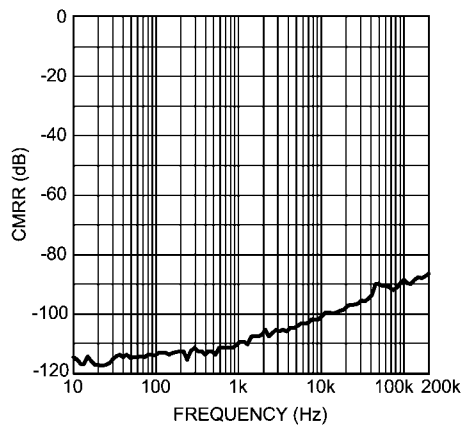
201572o8

CMRR vs Frequency
 $V_{CC} = 12V$, $V_{EE} = -12V$
 $R_L = 10k\Omega$



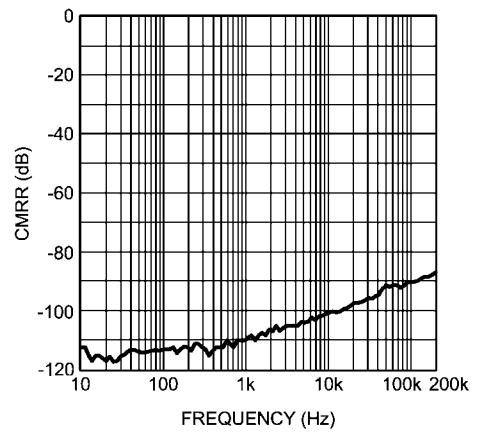
201572f8

CMRR vs Frequency
 $V_{CC} = 17V$, $V_{EE} = -17V$
 $R_L = 10k\Omega$



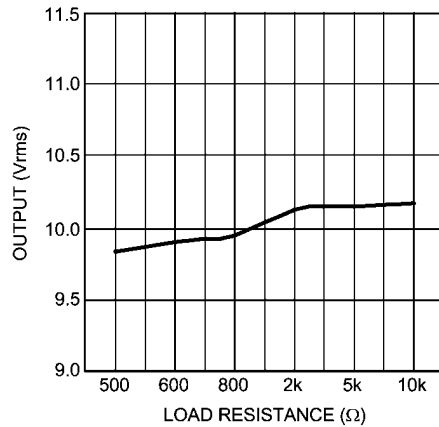
201572g4

CMRR vs Frequency
 $V_{CC} = 2.5V$, $V_{EE} = -2.5V$
 $R_L = 10k\Omega$



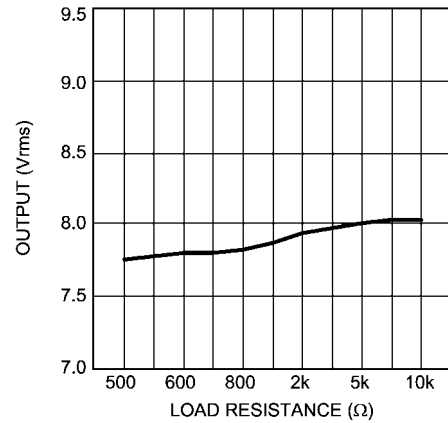
201572f5

Output Voltage vs Load Resistance
 $V_{DD} = 15V$, $V_{EE} = -15V$
 $THD+N = 1\%$



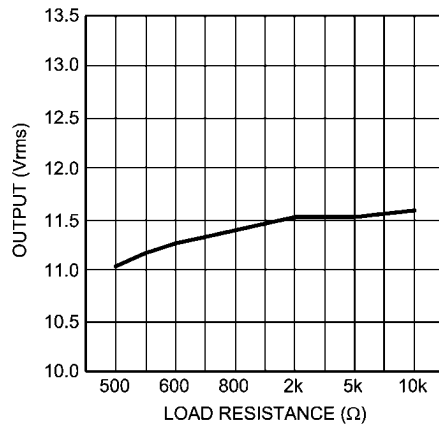
201572h1

Output Voltage vs Load Resistance
 $V_{DD} = 12V$, $V_{EE} = -12V$
 $THD+N = 1\%$



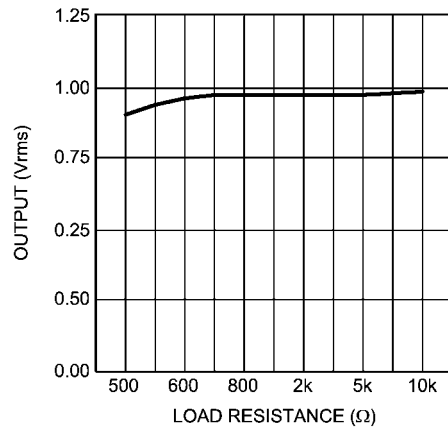
201572h0

Output Voltage vs Load Resistance
 $V_{DD} = 17V$, $V_{EE} = -17V$
 $THD+N = 1\%$

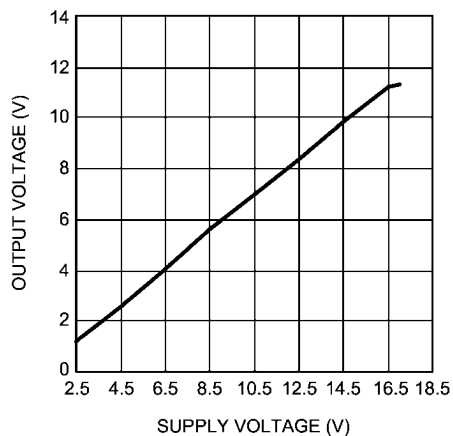


201572h2

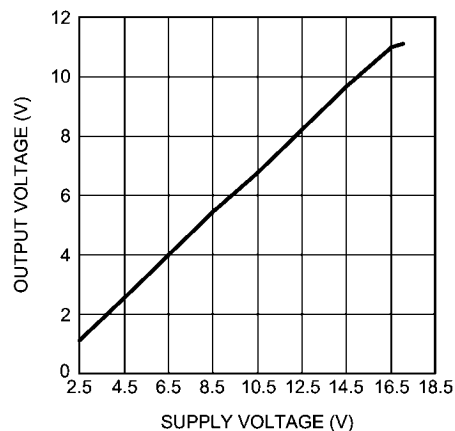
Output Voltage vs Load Resistance
 $V_{DD} = 2.5V$, $V_{EE} = -2.5V$
 $THD+N = 1\%$



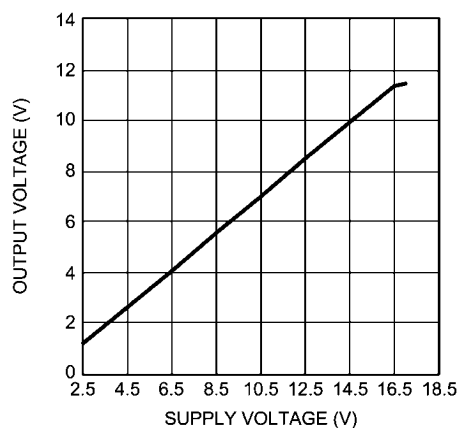
201572g9

Output Voltage vs Supply Voltage $R_L = 2k\Omega$, THD+N = 1%

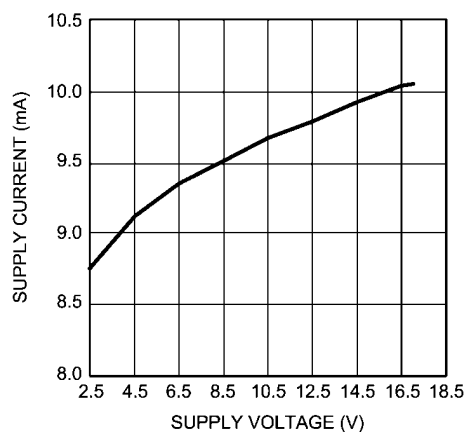
201572j9

Output Voltage vs Supply Voltage $R_L = 600\Omega$, THD+N = 1%

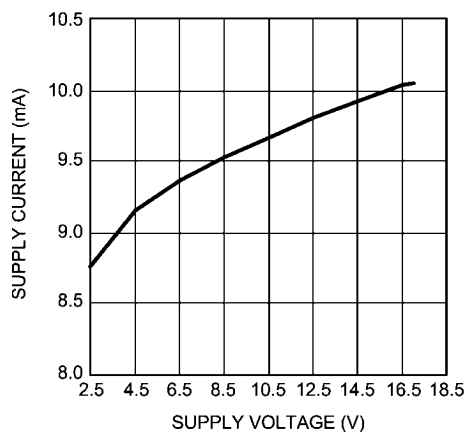
201572j8

Output Voltage vs Supply Voltage $R_L = 10k\Omega$, THD+N = 1%

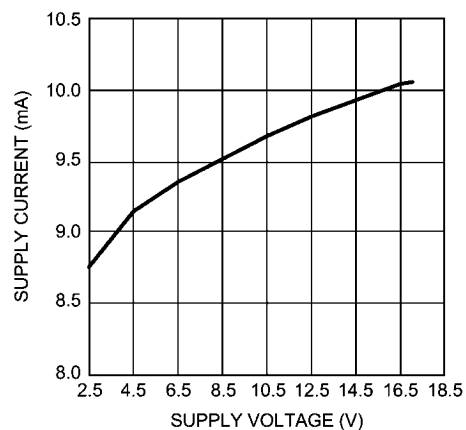
201572k0

Supply Current vs Supply Voltage $R_L = 2k\Omega$ 

201572j6

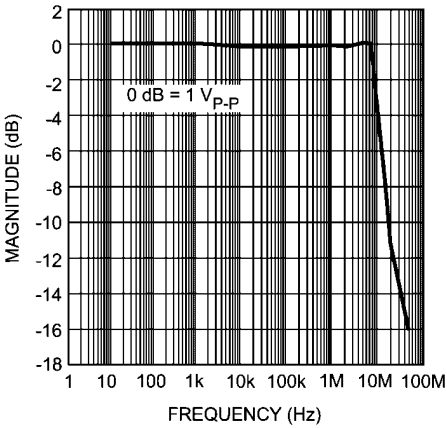
Supply Current vs Supply Voltage $R_L = 600\Omega$ 

201572j5

Supply Current vs Supply Voltage $R_L = 10k\Omega$ 

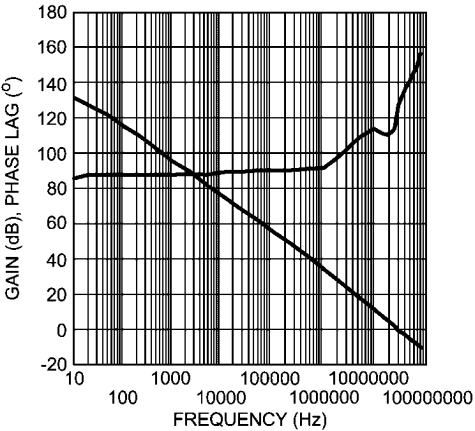
201572j7

Full Power Bandwidth vs Frequency



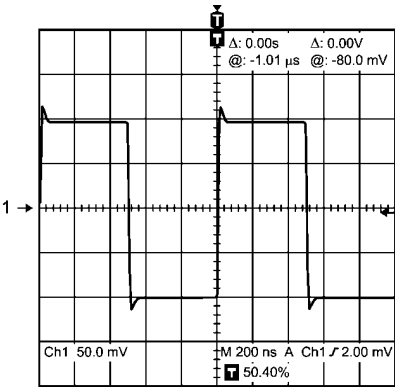
201572j0

Gain Phase vs Frequency



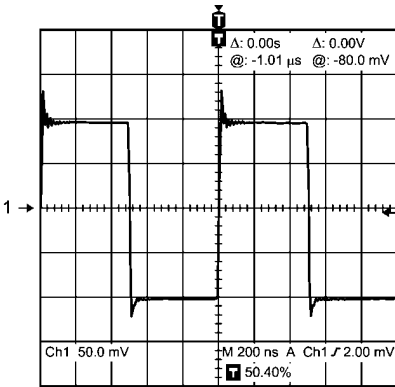
201572j1

Small-Signal Transient Response
 $A_v = 1$, $C_L = 10\text{pF}$



201572i7

Small-Signal Transient Response
 $A_v = 1$, $C_L = 100\text{pF}$



201572i8

Application Information

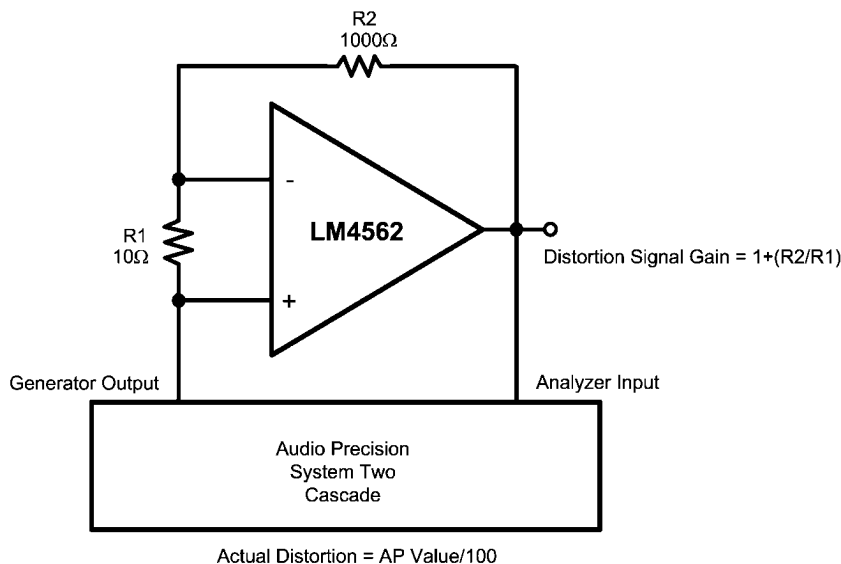
DISTORTION MEASUREMENTS

The vanishingly low residual distortion produced by LM4562 is below the capabilities of all commercially available equipment. This makes distortion measurements just slightly more difficult than simply connecting a distortion meter to the amplifier's inputs and outputs. The solution, however, is quite simple: an additional resistor. Adding this resistor extends the resolution of the distortion measurement equipment.

The LM4562's low residual distortion is an input referred internal error. As shown in Figure 1, adding the 10Ω resistor connected between the amplifier's inverting and non-inverting inputs changes the amplifier's noise gain. The result is that

the error signal (distortion) is amplified by a factor of 101. Although the amplifier's closed-loop gain is unaltered, the feedback available to correct distortion errors is reduced by 101, which means that measurement resolution increases by 101. To ensure minimum effects on distortion measurements, keep the value of R1 low as shown in Figure 1.

This technique is verified by duplicating the measurements with high closed loop gain and/or making the measurements at high frequencies. Doing so produces distortion components that are within the measurement equipment's capabilities. This datasheet's THD+N and IMD values were generated using the above described circuit connected to an Audio Precision System Two Cascade.



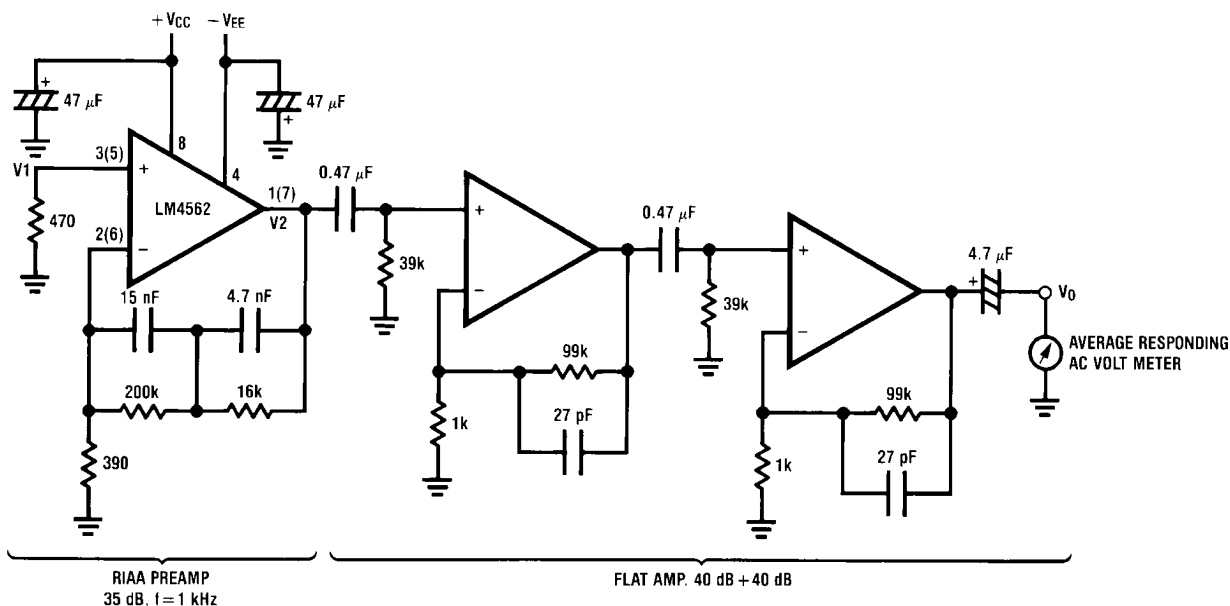
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FIGURE 1. THD+N and IMD Distortion Test Circuit

The LM4562 is a high speed op amp with excellent phase margin and stability. Capacitive loads up to 100pF will cause little change in the phase characteristics of the amplifiers and are therefore allowable.

Capacitive loads greater than 100pF must be isolated from the output. The most straightforward way to do this is to put

a resistor in series with the output. This resistor will also prevent excess power dissipation if the output is accidentally shorted.

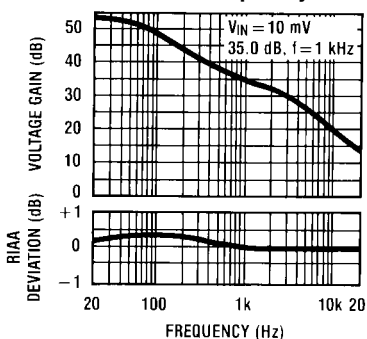


Complete shielding is required to prevent induced pick up from external sources. Always check with oscilloscope for power line noise.

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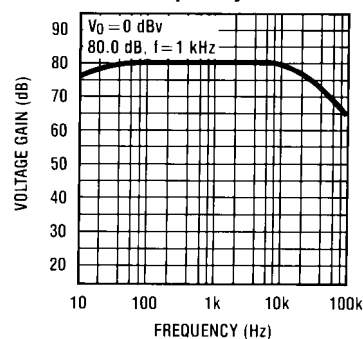
Noise Measurement Circuit
Total Gain: 115 dB @ $f = 1$ kHz
Input Referred Noise Voltage: $e_n = V_0/560,000$ (V)

RIAA Preamp Voltage Gain, RIAA Deviation vs Frequency



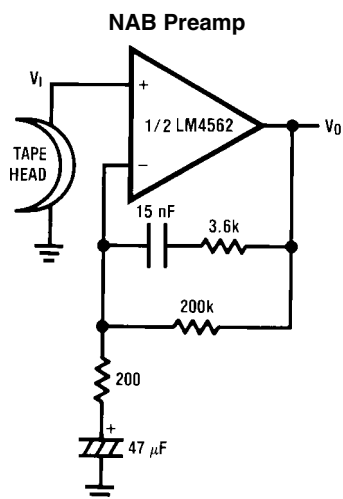
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Flat Amp Voltage Gain vs Frequency



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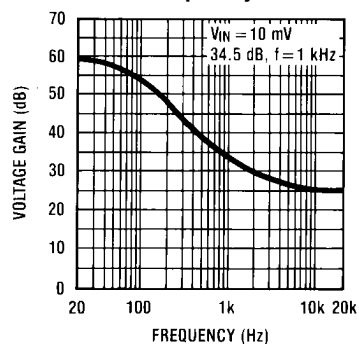
TYPICAL APPLICATIONS



$A_v = 34.5$
 $F = 1 \text{ kHz}$
 $E_n = 0.38 \mu\text{V}$
 A Weighted

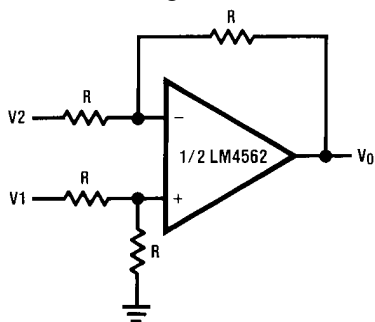
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NAB Preamp Voltage Gain vs Frequency



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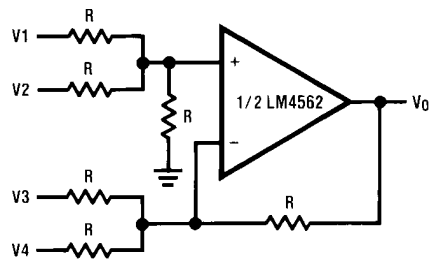
Balanced to Single Ended Converter



$$V_O = V_1 - V_2$$

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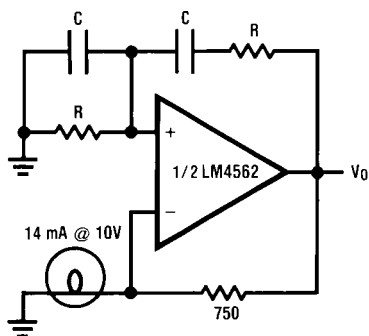
Adder/Subtractor



$$V_O = V_1 + V_2 - V_3 - V_4$$

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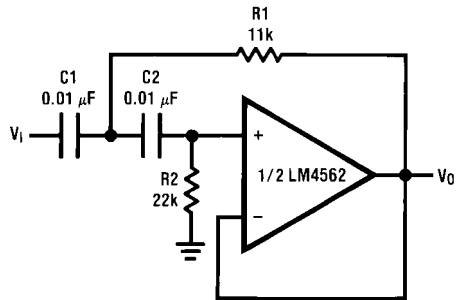
Sine Wave Oscillator



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$$f_o = \frac{1}{2\pi RC}$$

Second Order High Pass Filter (Butterworth)



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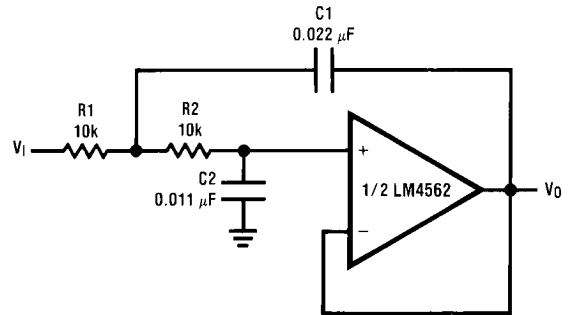
if $C1 = C2 = C$

$$R1 = \frac{\sqrt{2}}{2\omega_0 C}$$

$$R2 = 2 \cdot R1$$

Illustration is $f_0 = 1 \text{ kHz}$

Second Order Low Pass Filter (Butterworth)



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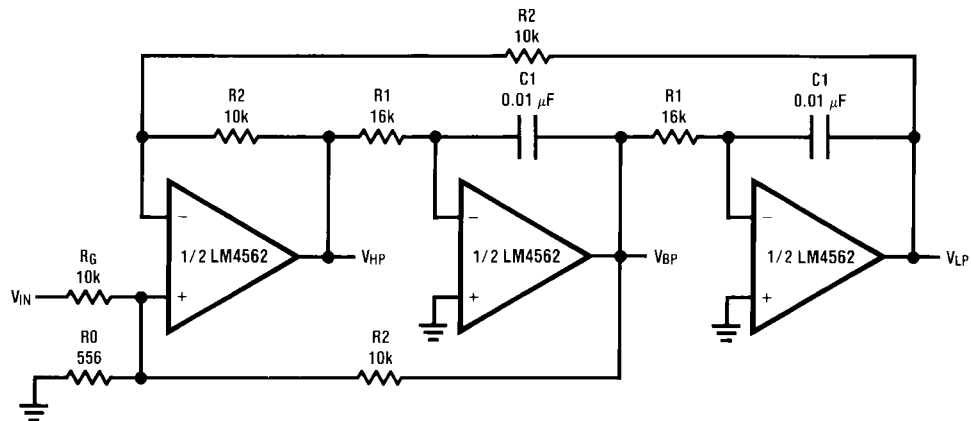
if $R1 = R2 = R$

$$C1 = \frac{\sqrt{2}}{\omega_0 R}$$

$$C2 = \frac{C1}{2}$$

Illustration is $f_0 = 1 \text{ kHz}$

State Variable Filter

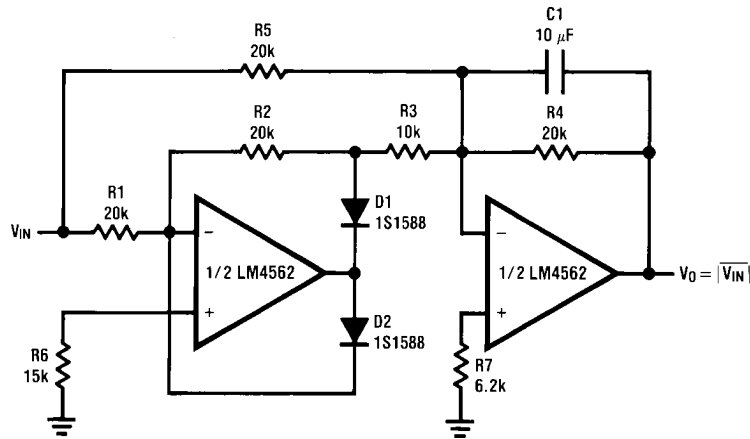


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$$f_0 = \frac{1}{2\pi C1 R1}, Q = \frac{1}{2} \left(1 + \frac{R2}{R0} + \frac{R2}{RG} \right), A_{BP} = Q A_{LP} = Q A_{LH} = \frac{R2}{RG}$$

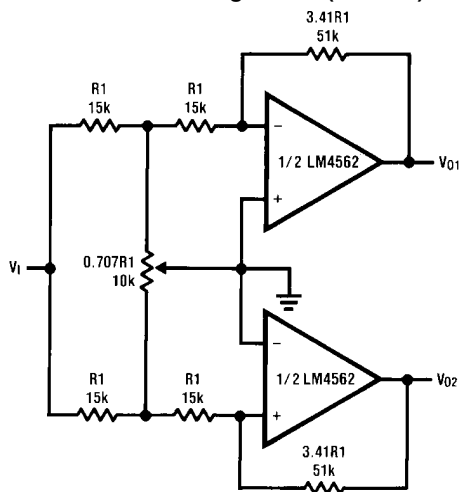
Illustration is $f_0 = 1 \text{ kHz}$, $Q = 10$, $A_{BP} = 1$

AC/DC Converter



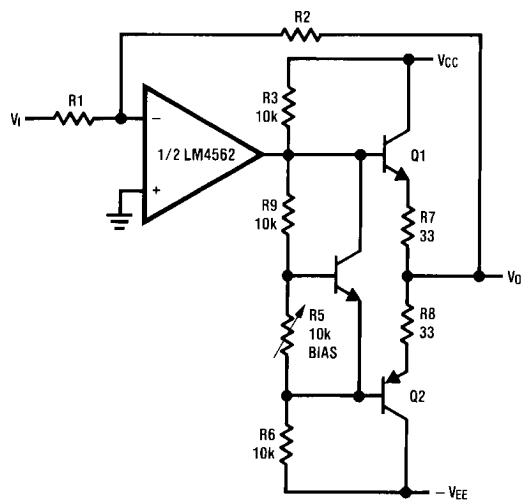
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2 Channel Panning Circuit (Pan Pot)



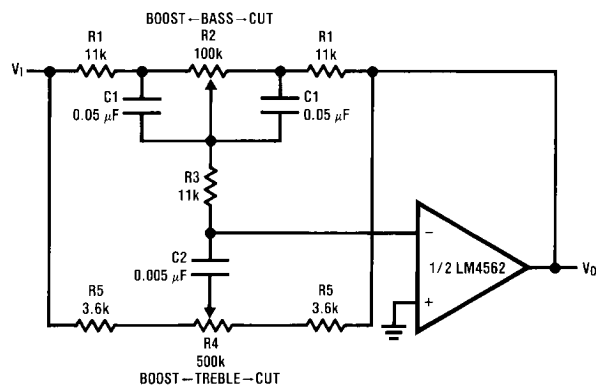
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Line Driver



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Tone Control



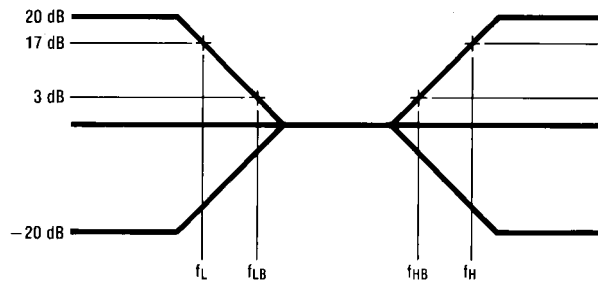
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$$f_L = \frac{1}{2\pi R2C1}, f_{LB} = \frac{1}{2\pi R1C1}$$

$$f_H = \frac{1}{2\pi R5C2}, f_{HB} = \frac{1}{2\pi (R1 + R5 + 2R3)C2}$$

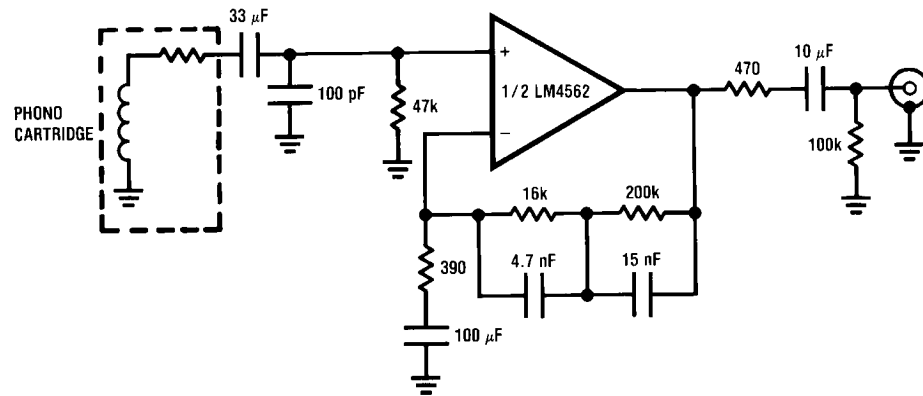
Illustration is:

$f_L = 32 \text{ Hz}$, $f_{LB} = 320 \text{ Hz}$
 $f_H = 11 \text{ kHz}$, $f_{HB} = 1.1 \text{ kHz}$



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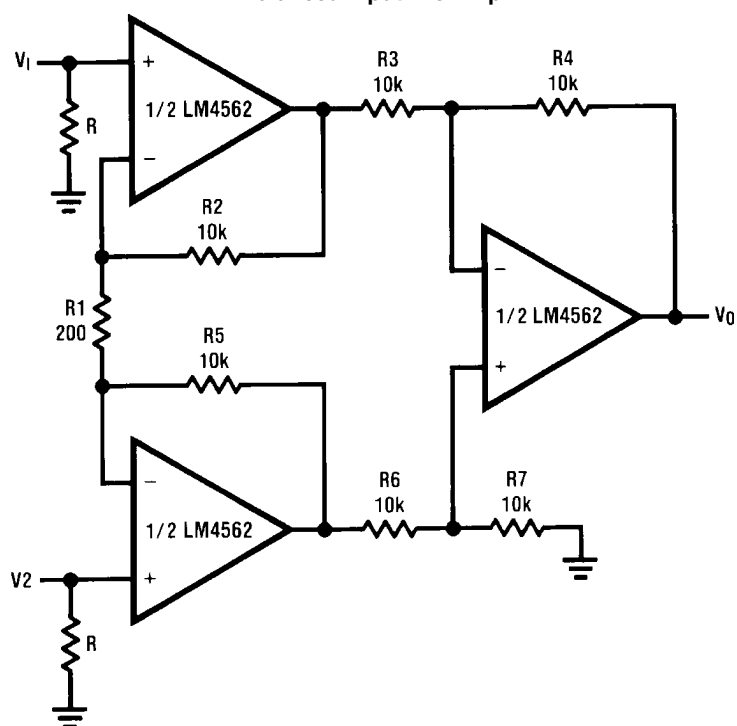
RIAA Preamp



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$A_v = 35 \text{ dB}$
 $E_n = 0.33 \mu\text{V}$
 $S/N = 90 \text{ dB}$
 $f = 1 \text{ kHz}$
 A Weighted
 A Weighted, $V_{IN} = 10 \text{ mV}$
 @ $f = 1 \text{ kHz}$

Balanced Input Mic Amp



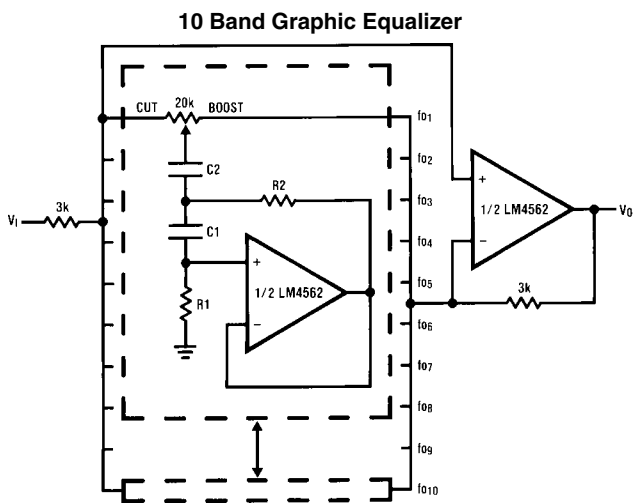
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If $R2 = R5$, $R3 = R6$, $R4 = R7$

$$V_0 = \left(1 + \frac{2R_2}{R_1}\right) \frac{R_4}{R_3} (V_2 - V_1)$$

Illustration is:

$$V_0 = 101(V_2 - V_1)$$



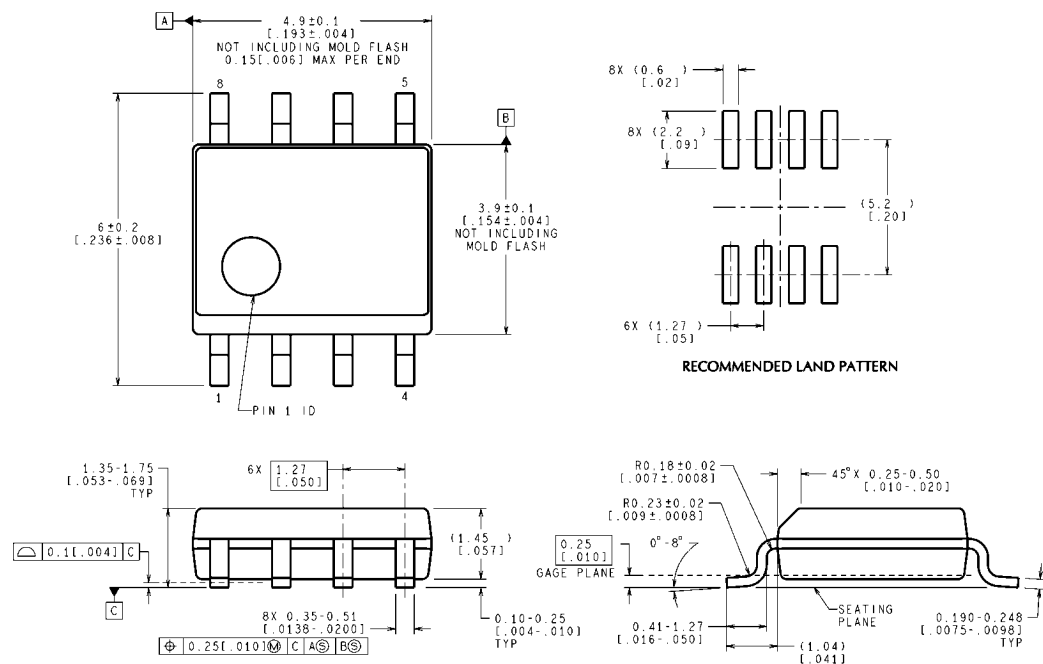
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fo (Hz)	C ₁	C ₂	R ₁	R ₂
32	0.12μF	4.7μF	75kΩ	500Ω
64	0.056μF	3.3μF	68kΩ	510Ω
125	0.033μF	1.5μF	62kΩ	510Ω
250	0.015μF	0.82μF	68kΩ	470Ω
500	8200pF	0.39μF	62kΩ	470Ω
1k	3900pF	0.22μF	68kΩ	470Ω
2k	2000pF	0.1μF	68kΩ	470Ω
4k	1100pF	0.056μF	62kΩ	470Ω
8k	510pF	0.022μF	68kΩ	510Ω
16k	330pF	0.012μF	51kΩ	510Ω

Note 9: At volume of change = ±12 dB
Q = 1.7
Reference: "AUDIO/RADIO HANDBOOK", National Semiconductor, 1980, Page 2–61

Revision History

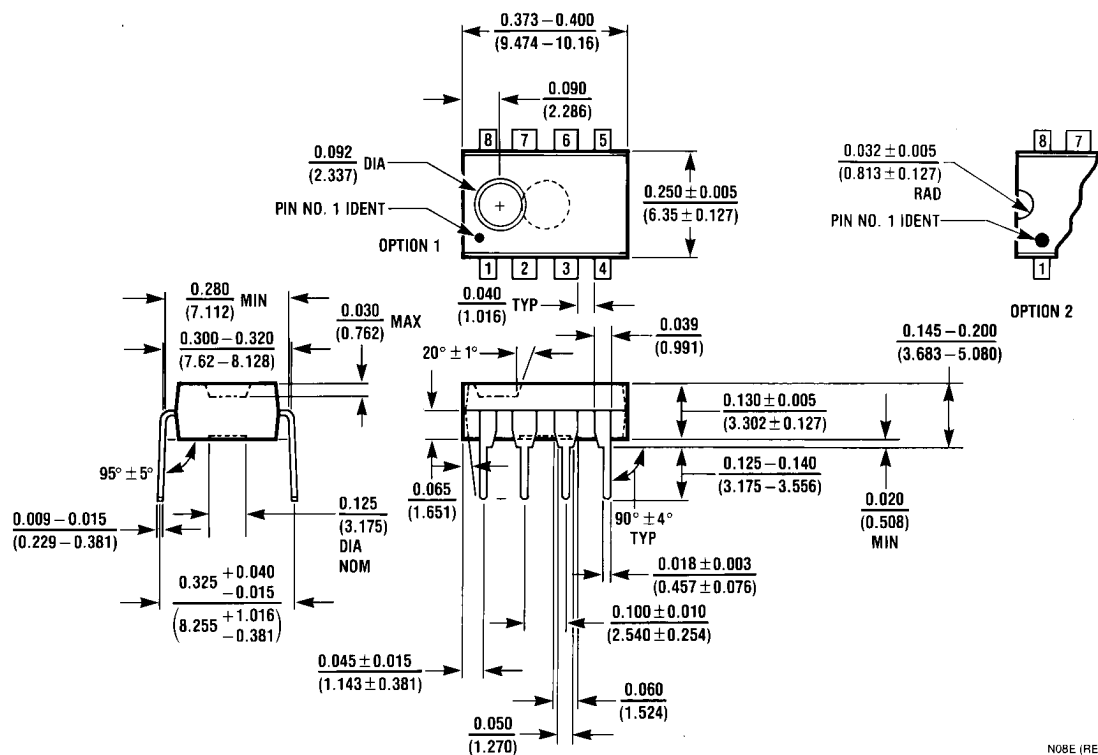
Rev	Date	Description
1.0	08/16/06	Initial release.
1.1	08/22/06	Updated the Instantaneous Short Circuit Current specification.
1.2	09/12/06	Updated the three $\pm 15\text{V}$ CMRR Typical Performance Curves.
1.3	09/26/06	Updated interstage filter capacitor values on page 1 Typical Application schematic.

Physical Dimensions inches (millimeters) unless otherwise noted

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VALUES IN [] ARE INCHES
DIMENSIONS IN () FOR REFERENCE ONLY

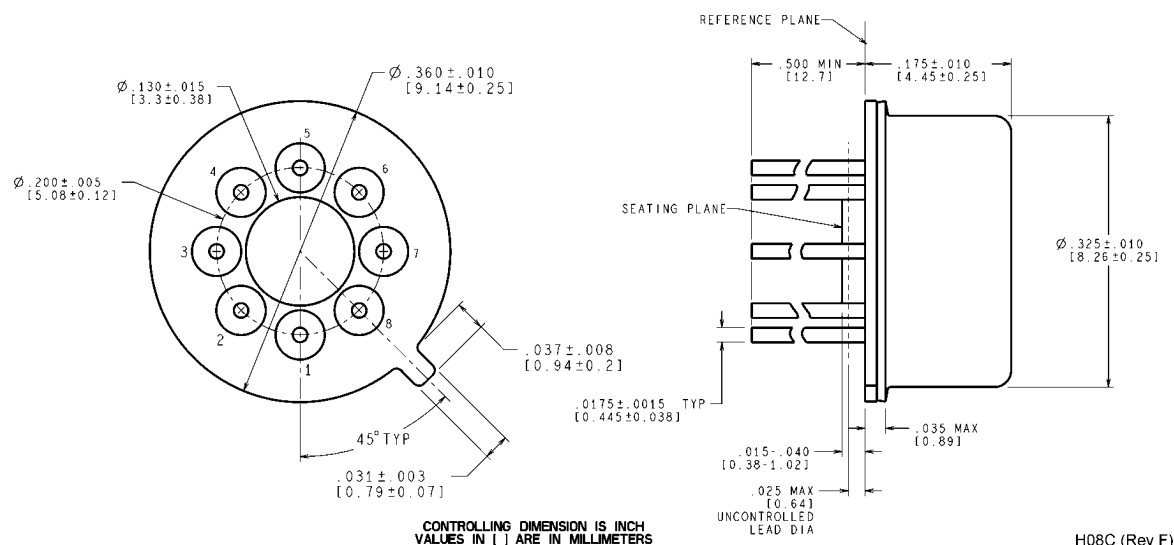
M08A (Rev L)

Narrow SOIC Package
Order Number LM4562MA
NS Package Number M08A



N08E (REV F)

Dual-In-Line Package
Order Number LM4562NA
NS Package Number N08E



H08C (Rev F)

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TO-99 Metal Can Package
Order Number LM4562HA
NS Package Number H08C

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